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► **To cite this version:**

Thierry Miquel, Jean-Marc Loscos, Francis Casaux, Felix Mora-Camino. Statistical performance evaluation between linear and nonlinear designs for aircraft relative guidance. ATM 2005, 6th USA/Europe Air Traffic Management Research and Development Seminar, Jun 2005, Baltimore, United States. pp xxxx. hal-00938078

**HAL Id: hal-00938078**

**<https://enac.hal.science/hal-00938078>**

Submitted on 27 May 2014

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# STATISTICAL PERFORMANCE EVALUATION BETWEEN LINEAR AND NONLINEAR DESIGNS FOR AIRCRAFT RELATIVE GUIDANCE

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## Abstract

Over the last few years, several concepts concerning the delegation to the flight crew of some tasks currently performed by the air traffic controllers have emerged. Among these new ideas, relative guidance has appeared to be capable to contribute to the enhancement of air traffic capacity though it raises difficult technical challenges. Indeed, this kind of maneuver appears difficult to perform manually, and may induce an excessive increase in flight crew workload, thus requiring new on-board automated functions. Some linear and nonlinear techniques have already been applied to design a feedback loop which performs automatically merging maneuvers and maintains station keeping behind a designated aircraft. The main contributions of the paper consist in a new nonlinear design of the feedback control loop and in the comparison between a linear design and the proposed nonlinear design, namely a proportional/derivative design and the proposed backstepping design. The comparison is based on Monte Carlo simulations, and promotes the nonlinear design. Indeed, a touch of complexity in the design process allows for better performances: backstepping fosters quick achievement of merging and station keeping maneuvers.

## Introduction

The main task of air traffic controllers managing arrival traffic is to sequence, merge and space aircraft for landing. An example of typical flight path for arriving aircraft at an airport is shown in Figure 1:

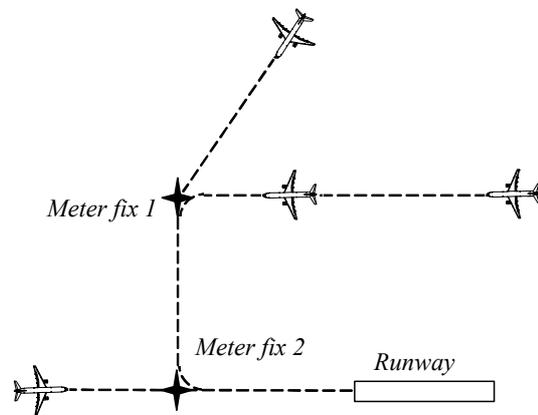


Figure 1. Example of sequencing and merging operations for arriving aircraft at airport

When one aircraft crosses the meter fixes, the following aircraft must be spaced at a prescribed minimum distance or time behind. Indeed, aircraft shall always be protected at least from wake turbulence generated by other aircraft. The minimum wake turbulence separation adopted by the civil aviation authorities depends upon the maximum takeoff weights of the aircraft involved ([1]).

The task of establishing properly spaced landing sequences is very demanding for air traffic controllers under heavy traffic conditions. As a consequence, automation tools named Arrival Manager (*AMAN*) often help air traffic controllers to build a sequence of aircraft in order to safely and expeditiously land them ([2]). Unfortunately, the airborne counterpart of the arrival manager which could help the flight crew to merge its aircraft towards a meter fix according to a sequence constraint is not yet available. Indeed, despite the fact that current aircraft's Flight Management Systems (*FMS*) have the ability to navigate over predefined

paths, they are not capable of meeting a specified time-lag over meter fix *relatively* to another aircraft.

New concepts such as the delegation to the flight crew of some tasks presently performed by air traffic controllers have emerged during the last few years ([2]). More specifically, automatic merging and station keeping operations could relieve air traffic controllers of the need to provide time consuming radar vectoring instructions to the trailing aircraft once the flight crew has accepted the relative guidance clearance. Thus, the expected benefit of such new capabilities onboard aircraft is an increase of air traffic controller availability, which could result in increased air traffic efficiency and / or capacity. Enhancement of flight crew airborne traffic situational awareness with associated safety benefits is also expected.

As such a new capability onboard aircraft requires some surveillance and communication capabilities, and more specifically the knowledge of the leading aircraft position and velocity, the Automatic Dependent Surveillance-Broadcast (*ADS-B*) is a potential key enabler to support these surveillance requirements ([4]). Aircraft equipped with *ADS-B* capabilities broadcast their position, velocity and identification periodically (e.g. every second). Any neighboring aircraft capable of receiving those data will therefore be capable of tracking surrounding traffic.

Preliminary studies have mainly investigated the station keeping phase without taking into consideration the merging phase. This field is addressed for *UAVs* and military aircraft by means of linear feedback loop ([5]) or nonlinear feedback loop such as sliding mode control ([6]). However, research for civil aircraft where safety and passenger comfort are crucial issues is still in its initial stage. Indeed, [7] focuses on station keeping performed manually, whereas [8] develops a linear feedback loop (*PID*) limited to the control of longitudinal station keeping.

This paper investigates a linear and a *new* nonlinear design for both merging at a specified meter fix and station keeping. Eventually it compares both designs. This paper is the result of a joined effort between the French Air Navigation Study Center (CENA) which brings the operational concept and the French National College of Aviation (ENAC) which brings the competences in automatic control.

The paper is organized as follows: in the first section dealing with relative motion kinematics, inertial position dynamics, relative position dynamics and state space representation are introduced. Subsequent sections deal with the design of the linear

and the nonlinear feedback loops. Then, the statistical performance evaluation is performed and conclusions are raised.

## Relative motion kinematics

### Inertial position dynamics

The considered reference frame is affixed to the current position of the trailing aircraft, as shown in Figure 2:

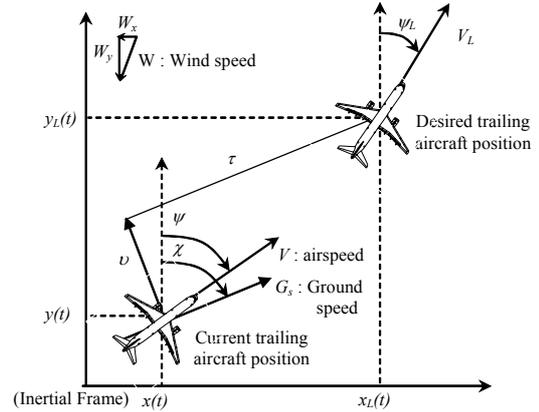


Figure 2. Reference frame

The along track distance, denoted by  $\tau$ , is aligned with the trailing aircraft ground speed vector, whereas the cross track distance, denoted by  $\nu$ , is the distance from the current trailing aircraft position to the desired trailing aircraft position (i.e. the leading aircraft position a few minutes earlier) perpendicularly to its ground speed. The heading angle of the trailing aircraft is denoted by  $\psi$ , its airspeed by  $V$ . Subscript  $L$  is added for all variables related to the desired state vector.

Since wind is considered in this paper, the track angle  $\chi$  and the ground speed  $G_s$  are related to the inertial velocity as follows:

$$\begin{cases} \dot{x} = G_s \cdot \sin(\chi) \\ \dot{y} = G_s \cdot \cos(\chi) \end{cases} \quad (1)$$

Assuming that Earth is flat and non-rotating, it may be considered as an inertial frame. From Figure 2, the inertial position dynamics of the trailing aircraft are given by the following relations, where  $\psi_w$  denotes the direction *from* where the wind is blowing and  $W$  its velocity:

$$\begin{cases} \dot{x} = V \cdot \sin(\psi) + W \cdot \sin(\psi_w - \pi) \\ \dot{y} = V \cdot \cos(\psi) + W \cdot \cos(\psi_w - \pi) \end{cases} \quad (2)$$

Those relations hold even if the motion of the aircraft in the vertical plane is considered as far as the

flight path angle  $\gamma$  is small, which is a realistic assumption for commercial aircraft.

Referring to (1) and (2), the track angle  $\chi$  and the heading angle  $\psi$  are linked by the following relations:

$$\begin{cases} \chi = \arctan\left(\frac{V \cdot \sin(\psi) - W \cdot \sin(\psi_w)}{V \cdot \cos(\psi) - W \cdot \cos(\psi_w)}\right) \\ G_s = \sqrt{V^2 + W^2 - 2 \cdot V \cdot W \cdot \cos(\psi - \psi_w)} \end{cases} \quad (3)$$

### Relative position dynamics

From Figure 2, the trailing aircraft desired position relatively to the current position of the trailing aircraft can be expressed in terms of the inertial positions as follows:

$$\begin{cases} \tau(t) = (x_L(t) - x(t)) \cdot \sin(\chi) + (y_L(t) - y(t)) \cdot \cos(\chi) \\ \upsilon(t) = (x_L(t) - x(t)) \cdot \cos(\chi) - (y_L(t) - y(t)) \cdot \sin(\chi) \end{cases} \quad (4)$$

Taking into account the inertial position dynamics expressed in (2), and assuming the same wind for the leading and the trailing aircraft, the time derivative of (4) yields:

$$\begin{cases} \dot{\tau} = \dot{\chi} \cdot \upsilon + V_L \cdot \cos(\psi_L - \chi) - V \cdot \cos(\psi - \chi) \\ \dot{\upsilon} = -\dot{\chi} \cdot \tau + V_L \cdot \sin(\psi_L - \chi) - V \cdot \sin(\psi - \chi) \end{cases} \quad (5)$$

The time derivative  $\dot{\chi}$  is obtained by differentiating (3). As far as the track angle  $\chi$  is a function of  $(V, \psi)$ , its time derivative is a function of  $(\dot{V}, \dot{\psi}, \dot{\psi}_w, \dot{\psi}_w)$ . Note that it also depends on the wind characteristics  $(W, \dot{W}, \psi_w, \dot{\psi}_w)$  that are generally available on-board through the Air Data Computer (ADC).

### State space representation

Denoting by  $\mathbf{u}$  the control vector, by  $\mathbf{x}_1$  and  $\mathbf{x}_2$  the state vectors, and assuming that  $(W, \dot{W}, \psi_w, \dot{\psi}_w)$  and  $(V_L, \psi_L)$  are exogenous variable, equations (5) reduce to the following state space representation of the relative guidance kinematics:

$$\begin{cases} \dot{\mathbf{x}}_1 = A(\mathbf{x}_2, \mathbf{u}) \cdot \mathbf{x}_1 + B(\mathbf{x}_2) \\ \dot{\mathbf{x}}_2 = \mathbf{u} \end{cases} \quad (6)$$

where the state vectors  $\mathbf{x}_1$  and  $\mathbf{x}_2$  and the control vector  $\mathbf{u}$  are defined by:

$$\begin{cases} \mathbf{x}_1 = [\tau \quad \upsilon]^T \\ \mathbf{x}_2 = [\psi \quad V]^T \\ \mathbf{u} = [\dot{\psi} \quad \dot{V}]^T \end{cases} \quad (7)$$

and:

$$\begin{cases} A(\mathbf{x}_2, \mathbf{u}) = \begin{bmatrix} 0 & \dot{\chi}(\mathbf{x}_2, \mathbf{u}) \\ -\dot{\chi}(\mathbf{x}_2, \mathbf{u}) & 0 \end{bmatrix} \\ B(\mathbf{x}_2) = \begin{bmatrix} V_L \cdot \cos(\psi_L - \chi) - V \cdot \cos(\psi - \chi) \\ V_L \cdot \sin(\psi_L - \chi) - V \cdot \sin(\psi - \chi) \end{bmatrix} \end{cases} \quad (8)$$

It is worth noticing that vector  $B(\mathbf{x}_2)$  can also be written according to the ground parameters:

$$B(\mathbf{x}_2) = \begin{bmatrix} G_{sL} \cdot \cos(\chi_L - \chi) - G_s \\ G_{sL} \cdot \sin(\chi_L - \chi) \end{bmatrix} \quad (9)$$

This state space representation will be used for both the linear and nonlinear feedback loop designs, which are presented in the next paragraphs.

### Linear feedback loop design

The design objective is to render the equilibrium points  $\mathbf{x}_{1e} = [0 \quad 0]^T$  and  $\mathbf{x}_{2e} = [\psi_L \quad V_L]^T$  globally asymptotically stable.

Since system (6) is nonlinear, a first alternative to design a feedback loop which stabilizes the system around equilibrium points  $\mathbf{x}_{1e}$  and  $\mathbf{x}_{2e}$  consists in linearizing the system. This is clearly a local approach, but it is the classical way to approach the stabilization problem for nonlinear systems ([9]).

Linearization of system (6) about  $\mathbf{x}_{1e}$  and  $\mathbf{x}_{2e}$  results in the following linear system:

$$\begin{cases} \dot{\mathbf{x}}_1 = \left. \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \right|_{\mathbf{x}_2 = \mathbf{x}_{2e}} \cdot (\mathbf{x}_2 - \mathbf{x}_{2e}) = \hat{B} \cdot (\mathbf{x}_2 - \mathbf{x}_{2e}) \\ \dot{\mathbf{x}}_2 = \mathbf{u} \end{cases} \quad (10)$$

where:

$$\hat{B} = \begin{bmatrix} V_L \sin(\psi_L - \chi_L) & -\cos(\psi_L - \chi_L) \\ -V_L \cos(\psi_L - \chi_L) & -\sin(\psi_L - \chi_L) \end{bmatrix} \quad (11)$$

As far as the state vectors  $\mathbf{x}_1$  and  $\mathbf{x}_2$  are available for feedback and the linearized system is completely state controllable, a pole placement technique can be applied in order to place the poles of the closed loop system at any desired location. To this end, the time derivative of the state vector  $\mathbf{x}_1$  is derived once again:

$$\ddot{\mathbf{x}}_1 = \hat{B} \cdot \dot{\mathbf{x}}_2 = \hat{B} \cdot \mathbf{u} \quad (12)$$

Now that the control vector  $\mathbf{u}$  appears explicitly from the time derivative of the output vector  $\mathbf{x}_1$ , the dynamics of vector  $\mathbf{x}_1$  is chosen so that it converges towards the equilibrium point  $\mathbf{x}_{1e}$ . To that end, vector  $\mathbf{x}_1$  may obey to a second order linear differential equation, where  $\Lambda_p$  and  $\Lambda_d$  stand for positive definite feedback gain matrices (tuning parameters):

$$\ddot{\mathbf{x}}_1 = -\Lambda_d \dot{\mathbf{x}}_1 - \Lambda_p \mathbf{x}_1 \quad (13)$$

Gathering equations (3) and (4) leads to the expression of the control vector  $\mathbf{u}$ :

$$\mathbf{u} = -\hat{B}^{-1}(\Lambda_d \dot{\mathbf{x}}_1 + \Lambda_p \mathbf{x}_1) \quad (14)$$

where:

$$\hat{B}^{-1} = \begin{bmatrix} \sin(\psi_L - \chi_L)/V_L & -\cos(\psi_L - \chi_L)/V_L \\ -\cos(\psi_L - \chi_L) & -\sin(\psi_L - \chi_L) \end{bmatrix} \quad (15)$$

This resulting proportional and derivative (PD) feedback loop is time varying since matrix  $\hat{B}^{-1}$  is not constant and evolves with heading and airspeed of the leading aircraft.

Using the first equation of (10), the feedback loop (14) is expressed in function of the available state vector  $\mathbf{x}_1$  and  $\mathbf{x}_2$ :

$$\mathbf{u} = -\hat{B}^{-1}(\Lambda_d \cdot \hat{B} \cdot (\mathbf{x}_2 - \mathbf{x}_{2e}) + \Lambda_p \mathbf{x}_1) \quad (16)$$

Coefficients of matrix  $\Lambda_d$  have the dimension of  $sec^{-1}$  whereas coefficients of matrix  $\Lambda_p$  have the dimension of  $sec^{-2}$ .

## Nonlinear feedback loop design

Since the nonlinear system (6) consists of two cascaded systems with state vectors  $\mathbf{x}_1$  and  $\mathbf{x}_2$ , and taking into account the fact that the matrix  $A(\mathbf{x}_2, \mathbf{u})$  is skew-symmetric, the recent vectorial backstepping design methodology ([10]) for construction of both feedback control law and associated Lyapunov functions can be applied to stabilize the system around the equilibrium points  $\mathbf{x}_{1e}$  and  $\mathbf{x}_{2e}$ .

In a first step, the virtual control  $B(\mathbf{x}_2)$  is chosen in order to stabilize  $\mathbf{x}_1$  around the equilibrium point  $\mathbf{x}_{1e}$ :

$$B(\mathbf{x}_2) = \mathbf{z}_2 - \Lambda_1 \mathbf{x}_1 \quad (17)$$

where  $\Lambda_1$  stands for a positive definite feedback gain matrix (tuning parameter) and  $\mathbf{z}_2$  is a new state variable.

Then, a candidate Lyapunov function denoted by  $L_1$  is introduced for the  $\mathbf{x}_1$ -system, where  $k_1$  stands for a positive parameter:

$$L_1(\mathbf{x}_1) = \frac{k_1}{2} \mathbf{x}_1^T \mathbf{x}_1 \quad (18)$$

Taking into account (17) and the fact that the matrix  $A(\mathbf{x}_2, \mathbf{u})$  is skew-symmetric, the time derivative of (18) is:

$$\dot{L}_1(\mathbf{x}_1) = -k_1 \mathbf{x}_1^T \Lambda_1 \mathbf{x}_1 + k_1 \mathbf{z}_2^T \mathbf{x}_1 \quad (19)$$

In a second step, the dynamics of  $\mathbf{z}_2$  is obtained by time differentiation of (17). Taking into account (6) leads to:

$$\frac{dB(\mathbf{x}_2)}{dt} = \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \mathbf{u} = \dot{\mathbf{z}}_2 - \Lambda_1 \dot{\mathbf{x}}_1 \quad (20)$$

A candidate Lyapunov function for the whole model is:

$$L_2(\mathbf{x}_1, \mathbf{z}_2) = L_1(\mathbf{x}_1) + \frac{1}{2} \mathbf{z}_2^T \mathbf{z}_2 \quad (21)$$

Taking into account (6) and (20), the time derivative of (21) is:

$$\dot{L}_2(\mathbf{x}_1, \mathbf{z}_2) = \dot{L}_1(\mathbf{x}_1) + \mathbf{z}_2^T \left( \Lambda_1 \dot{\mathbf{x}}_1 + \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \mathbf{u} \right) \quad (22)$$

Finally, taking into account (19) leads to the following:

$$\dot{L}_2(\mathbf{x}_1, \mathbf{z}_2) = -k_1 \mathbf{x}_1^T \Lambda_1 \mathbf{x}_1 + \mathbf{z}_2^T \left( k_1 \mathbf{x}_1 + \Lambda_1 \dot{\mathbf{x}}_1 + \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \mathbf{u} \right) \quad (23)$$

The matrix  $\frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2}$  has the following expression:

$$\frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} = \begin{bmatrix} f(\mathbf{x}_2) & g(\mathbf{x}_2) \\ h(\mathbf{x}_2) & k(\mathbf{x}_2) \end{bmatrix} \quad (24)$$

Where:

$$\left\{ \begin{array}{l} f(\mathbf{x}_2) = V \sin(\psi - \chi) \\ \quad + \frac{\partial \chi}{\partial \psi} (V_L \sin(\psi_L - \chi) - V \sin(\psi - \chi)) \\ g(\mathbf{x}_2) = -\cos(\psi - \chi) \\ \quad + \frac{\partial \chi}{\partial V} (V_L \sin(\psi_L - \chi) - V \sin(\psi - \chi)) \\ h(\mathbf{x}_2) = -V \cos(\psi - \chi) \\ \quad - \frac{\partial \chi}{\partial \psi} (V_L \cos(\psi_L - \chi) - V \cos(\psi - \chi)) \\ k(\mathbf{x}_2) = -\sin(\psi - \chi) \\ \quad - \frac{\partial \chi}{\partial V} (V_L \cos(\psi_L - \chi) - V \cos(\psi - \chi)) \end{array} \right. \quad (25)$$

The partial derivatives  $\partial \chi / \partial \psi$  and  $\partial \chi / \partial V$  are computed from (3).

Note that if wind is not considered (i.e.  $\chi = \psi$  and  $G_s = V$ ) the above expressions reduce to:

$$\left\{ \begin{array}{l} f(\mathbf{x}_2) = V_L \sin(\psi_L - \psi) \\ g(\mathbf{x}_2) = -1 \\ h(\mathbf{x}_2) = -V_L \cos(\psi_L - \psi) \\ k(\mathbf{x}_2) = 0 \end{array} \right. \quad (26)$$

The key point of the feedback loop design is that matrix  $\frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2}$  is invertible. Indeed, we have:

$$\left(\frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2}\right)^{-1} = \frac{1}{\Delta(\mathbf{x}_2)} \begin{bmatrix} k(\mathbf{x}_2) & -g(\mathbf{x}_2) \\ -h(\mathbf{x}_2) & f(\mathbf{x}_2) \end{bmatrix} \quad (27)$$

Where:

$$\Delta(\mathbf{x}_2) = -V_L \frac{\partial \mathcal{X}}{\partial \psi} \cos(\psi_L - \psi) \quad (28)$$

$$+ V \left( 1 - \frac{\partial \mathcal{X}}{\partial \psi} + V_L \frac{\partial \mathcal{X}}{\partial V} \sin(\psi_L - \psi) \right)$$

Finally, the control vector  $\mathbf{u}$  is defined in order to regulate the virtual output  $\mathbf{z}_2$  to zero. This design has been initiated in [11] and is based on the Young's inequality, namely:

$$xy \leq \frac{x^2 + y^2}{2} \quad (29)$$

Taking into account (17) and the first equation of (6) into (23) leads to:

$$\dot{L}_2(\mathbf{x}_1, \mathbf{z}_2) = -k_1 \mathbf{x}_1^T \Lambda_1 \mathbf{x}_1 \quad (30)$$

$$+ \mathbf{z}_2^T (k_1 \mathbf{I}_2 + \Lambda_1 A(\mathbf{x}_2, \mathbf{u})) \mathbf{x}_1$$

$$+ \mathbf{z}_2^T \left( \Lambda_1 B(\mathbf{x}_2) + \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \mathbf{u} \right)$$

Matrix  $\mathbf{I}_2$  stands for identity matrix. For the specific case studied in this paper, we will assume that matrix  $\Lambda_1$  is diagonal:

$$\Lambda_1 = \text{diag}\{\lambda_{11}, \lambda_{12}\} \quad (31)$$

As a consequence, the use of the Young's inequality leads to:

$$\mathbf{z}_2^T (k_1 \mathbf{I}_2 + \Lambda_1 A(\mathbf{x}_2, \mathbf{u})) \mathbf{x}_1 \leq \frac{1}{2} \mathbf{x}_1^T K_1 \mathbf{x}_1 + \frac{1}{2} \mathbf{z}_2^T K_2 \mathbf{z}_2 \quad (32)$$

where  $K_1$  and  $K_2$  are positive definite diagonal matrices:

$$K_1 = \begin{bmatrix} k_1 + \lambda_{12} |\dot{\chi}| & 0 \\ 0 & k_1 + \lambda_{11} |\dot{\chi}| \end{bmatrix} \quad (33)$$

$$K_2 = \begin{bmatrix} k_1 + \lambda_{11} |\dot{\chi}| & 0 \\ 0 & k_1 + \lambda_{12} |\dot{\chi}| \end{bmatrix} \quad (34)$$

Therefore (29) becomes:

$$\dot{L}_2(\mathbf{x}_1, \mathbf{z}_2) \leq -\mathbf{x}_1^T \left( k_1 \Lambda_1 - \frac{K_1}{2} \right) \mathbf{x}_1 \quad (35)$$

$$+ \mathbf{z}_2^T \left( \frac{K_2}{2} \mathbf{z}_2 + \Lambda_1 B(\mathbf{x}_2) + \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \mathbf{u} \right)$$

In order to stabilize the  $(\mathbf{x}_1 - \mathbf{z}_2)$  system, the control vector  $\mathbf{u}$  is chosen as follows, where  $\Lambda_2$  stands for a positive definite feedback gain matrix (tuning parameter):

$$\mathbf{u} = - \left( \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \right)^{-1} \left( \left( \frac{K_2}{2} + \Lambda_2 \right) \mathbf{z}_2 + \Lambda_1 B(\mathbf{x}_2) \right) \quad (36)$$

Thus the time derivative of the candidate Lyapunov function becomes:

$$\dot{L}_2(\mathbf{x}_1, \mathbf{z}_2) \leq -\mathbf{x}_1^T \left( k_1 \Lambda_1 - \frac{K_1}{2} \right) \mathbf{x}_1 - \mathbf{z}_2^T \Lambda_2 \mathbf{z}_2 \quad (37)$$

The time derivative of the candidate Lyapunov function  $L_2$  can be made negative definite by choosing  $k_1$  and  $K_1$  such that:

$$k_1 \Lambda_1 - \frac{K_1}{2} > 0 \quad (38)$$

This choice is always possible. Parameter  $k_1$  has the dimension of  $\text{sec}^{-2}$ , whereas matrices  $\Lambda_1$  and  $\Lambda_2$  have the dimension of  $\text{sec}^{-1}$ .

Using equation (17), the feedback loop (36) is expressed in function of the available state vector  $\mathbf{x}_1$  and  $\mathbf{x}_2$ :

$$\mathbf{u} = - \left( \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \right)^{-1} \left( \left( \frac{K_2}{2} + \Lambda_2 + \Lambda_1 \right) B(\mathbf{x}_2) \right. \quad (39)$$

$$\left. + \left( \frac{K_2}{2} + \Lambda_2 \right) \Lambda_1 \mathbf{x}_1 \right)$$

## Statistical performance evaluation

### Matching linear and nonlinear designs

In order to fairly compare the linear and the nonlinear designs, the matrices  $K_2$ ,  $\Lambda_1$ ,  $\Lambda_2$ ,  $\Lambda_p$  and  $\Lambda_d$  have been chosen so that the backstepping feedback loop (39) and the proportional and derivative feedback loop (16) simplify to the same feedback loop around the equilibrium point  $\mathbf{x}_{2e}$ . As a consequence, the following identification has been made:

$$\begin{cases} \left( \frac{K_2}{2} + \Lambda_2 \right) \Lambda_1 = \Lambda_p \\ \frac{K_2}{2} + \Lambda_2 + \Lambda_1 = \Lambda_d \end{cases} \quad (40)$$

In summary, the linear feedback loop is expressed as follows:

$$\mathbf{u} = -\hat{B}^{-1} \left( \Lambda_d \cdot \hat{B} \cdot (\mathbf{x}_2 - \mathbf{x}_{2e}) + \Lambda_p \mathbf{x}_1 \right) \quad (41)$$

Whereas the nonlinear feedback loop is:

$$\mathbf{u} = - \left( \frac{\partial B(\mathbf{x}_2)}{\partial \mathbf{x}_2} \right)^{-1} \left( \Lambda_d B(\mathbf{x}_2) + \Lambda_p \mathbf{x}_1 \right) \quad (42)$$

In order to comply with the time response of the airspeed and bank angle control channels for a wide body aircraft such as an Airbus A320 ([12]), the matrices  $\Lambda_p$  and  $\Lambda_d$  have been set as follows:

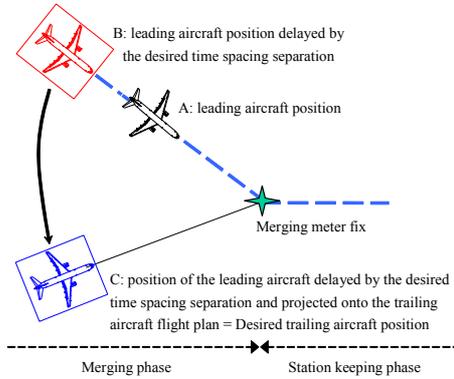
$$\begin{cases} \Lambda_p = \begin{bmatrix} 4 \cdot 10^{-4} & 0 \\ 0 & 4 \cdot 10^{-4} \end{bmatrix} \text{sec}^{-2} \\ \Lambda_d = \begin{bmatrix} 16 \cdot 10^{-3} & 0 \\ 0 & 16 \cdot 10^{-3} \end{bmatrix} \text{sec}^{-1} \end{cases} \quad (43)$$

It is assumed in the following that two decoupled autopilot functions dealing with airspeed control and bank angle control are available onboard the trailing aircraft. These decoupled functions assume coordination between throttle, aileron and rudder, as in many modern jets. In order to comply with the time response of the airspeed and bank angle control channels, the controlled airspeed and the controlled bank angle, denoted respectively by  $V_c$  and  $\phi_c$ , are set as follows during the simulations:

$$\begin{bmatrix} \phi_c \\ V_c \end{bmatrix} = \begin{bmatrix} 0 \\ V \end{bmatrix} + \begin{bmatrix} V/g & 0 \\ 0 & 50 \text{sec} \end{bmatrix} \mathbf{u} \quad (44)$$

### Relative guidance maneuver phases

The purpose of the relative guidance feedback loop is first to guide the trailing aircraft towards a merging meter fix and then to maintain station keeping behind the leading aircraft. As a consequence, the relative guidance maneuver is divided into two phases: the merging phase and the station keeping phase.



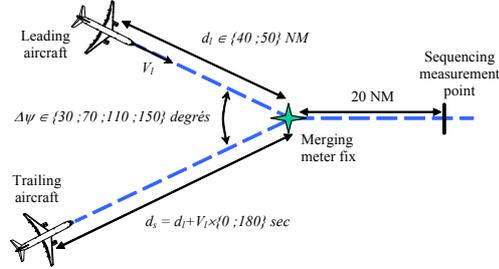
**Figure 3. Leading aircraft targeted position mapped to the flight plan of the trailing aircraft**

During the merging phase, and as shown in Figure 3, the current leading aircraft position (A) is delayed by the desired time spacing separation specified by air traffic control (B) and then projected onto the trailing aircraft flight plan (C). During this phase, the purpose of the relative guidance feedback loop is to track the delayed and projected leading aircraft position (position C).

As far as the delayed leading aircraft position has passed the merging meter fix, the projection onto the trailing aircraft flight plan is no more necessary.

### Encounters data base

On the basis of the encounter geometry presented in Figure 3, many encounters have been generated by changing the angle between the two convergence legs, the length of the merging leg for the leading aircraft and the aircraft type, as shown in Figure 4:



**Figure 4. Scenarios data base**

The encounters of the data base have been generated as follows:

- The angle between the two convergence legs varies between 30 and 150 degrees, with 40 degrees increment;
- The length of the merging leg for the leading aircraft is set either at 40 NM or 50 NM;
- Six different aircraft types have been selected from the Eurocontrol BADA database ([13]): ATR42/72, SAAB2000, A320, B767-300, A340, B747-400. Those types of aircraft are representative of the different type of propulsion, approach category and wake vortex category ([14]):

A/C type	ATR 42/72	SAAB2000	A320	B767-300	A340	B747-400
Propulsion	Turbo	Turbo	Jet	Jet	Jet	Jet
Approach Category	B	B	C	C	D	D
W. Vortex category	Med.	Med.	Med.	Heavy	Heavy	Heavy

**Table 1. Aircraft types**

- At the beginning of the encounter, aircraft start a descent at a flight level set between FL100 and FL260, as far as the selected flight level is flyable. They level off at FL100. The choice of the flight level sets the airspeed of the aircraft, which is compliant with the Eurocontrol BADA database ([13]) and varies between 266 kts and 492 kts;
- The initial position of the leading aircraft is set at a distance from the merging fix equal to  $d_l + V_l \times \{0; 180\}$  seconds, where  $d_l$  stands for the length of the leading aircraft merging leg and  $V_l$  for

the initial airspeed of the leading aircraft. As far as the objective for the relative guidance feedback loop is to place the following aircraft 90 seconds behind the leading aircraft, it shall delay or speed up the trailing aircraft by 90 seconds;

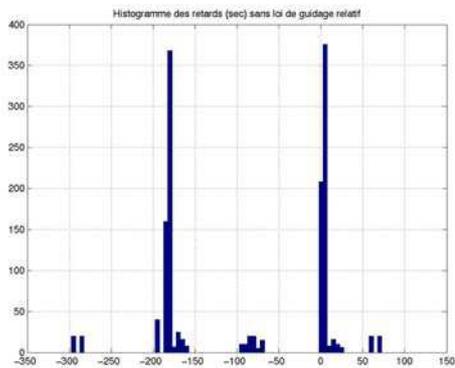
- A scenario is generated as far as the difference between the conventional airspeed of both aircraft is less than 30kts (airspeed compatibility) and as far as the expected distance to achieve the merging maneuver is greater than the actual distance between the initial position of the trailing aircraft and the point where the sequencing is measured.

Those considerations have led to the generation of 1408 encounters in the data base.

### Performance indicators

In order to assess the performances of both linear and nonlinear designs, three performance indicators have been computed:

- The first indicator is the delay between the leading and the trailing aircraft at the so-called sequencing measurement point. This point is placed 20 NM after the merging meter fix, where the station keeping phase is supposed to be achieved. This indicator is related with the quality of spacing. The histogram of this indicator for the encounter data base without any feedback loop is as follows:

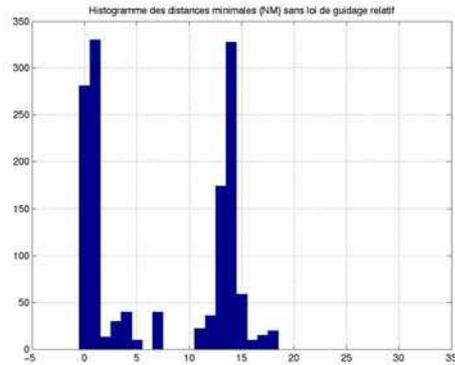


**Figure 5. Delay between the two aircraft at the sequencing measurement point without any feedback loop**

Without any feedback loop, the delay varies between -297 seconds and +71 seconds. The peaks of delays concentrate around values 0 and -180 seconds which are the values of delay chosen to calculate the initial position of the following aircraft. The variations around these values are due to the differences in speeds between the leader and the follower during the descent. The average of the delay

is -89 seconds, and the standard deviation is 97 seconds.

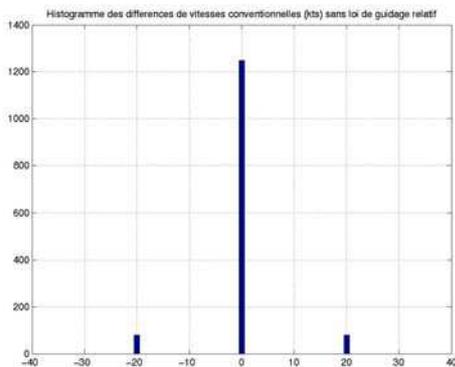
- The second indicator is the minimum distance between the two aircraft and is related with the safety of the relative guidance maneuver. The histogram of this indicator for the encounter data base without any feedback loop is as follows:



**Figure 6. Minimum distance between the two aircraft without any feedback loop**

The minimum distance varies between 0 and 18 NM. The two peaks correspond to the concentration of the delays around values 0 and -180 seconds. The average value of the minimal distance is 7.2 NM, and its standard deviation is 6.4 NM. There are 694 encounters for which the minimal distance is lower than 4.5 NM, and 624 encounters for which the minimal distance is lower than 2.5 NM.

- The third indicator relates to the dispersion of the difference between the conventional airspeed (CAS) of the leading and the trailing aircraft at the sequencing measurement point. This indicator is related to the operational acceptability of the relative guidance maneuver.

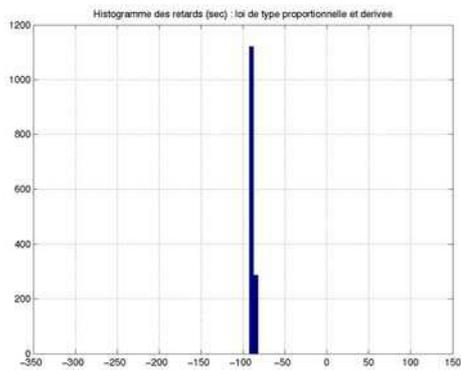


**Figure 7. Difference between the conventional airspeed of the two aircraft at the sequencing measurement point without any feedback loop**

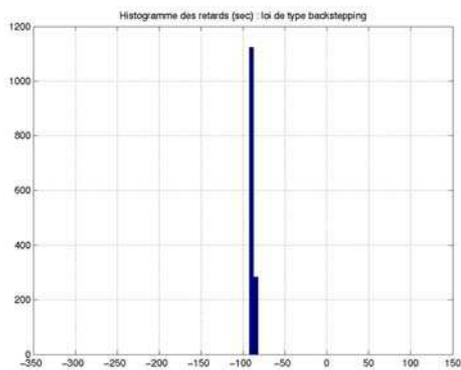
The histogram of this indicator for the encounter data base without any feedback loop is depicted on Figure 7. Most of the encounters occur with aircraft without any differences in conventional airspeed.

### ***Influence of linear and nonlinear feedback loops***

- The histogram of the delay between the leading and the trailing aircraft at the sequencing measurement point is represented on the following figures:



**Figure 8. Delay between the two aircraft at the sequencing measurement point with the linear feedback loop**

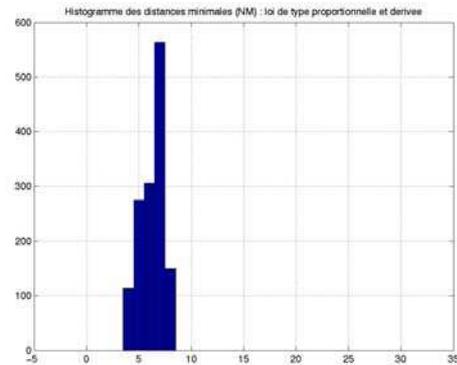


**Figure 9. Delay between the two aircraft at the sequencing measurement point with the nonlinear feedback loop**

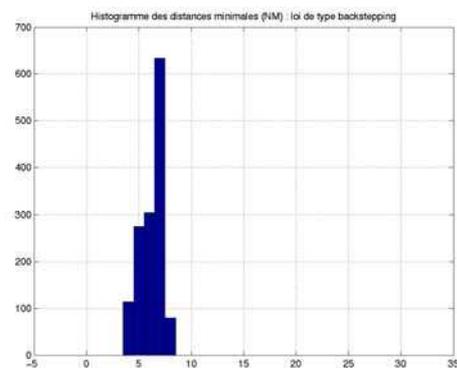
For the linear feedback loop, the delay varies between -91 seconds and -84 seconds. Its average is 88.6 seconds and the standard deviation is 1.6 seconds. For the nonlinear feedback loop, the delay varies between -91 seconds and -84 seconds. Its average is 88.8 seconds and the standard deviation is 2 seconds. As a consequence, the delay of 90 seconds between the two aircraft is achieved at the

sequencing measurement point for both linear and nonlinear feedback loop.

- The histogram of the minimum distance between the two aircraft is represented on the following figures:



**Figure 10. Minimum distance between the two aircraft with the linear feedback loop**



**Figure 11. Minimum distance between the two aircraft with the nonlinear feedback loop**

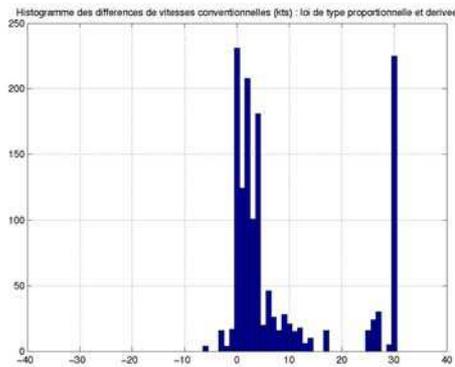
The peak of both histograms is located in the set of minimum distance ranging between 6.5 and 7.5 NM. This set corresponds to a true airspeed of 288 kts (that is a conventional airspeed of 250 kts at FL100, which is the usual procedure for the jets which represent the majority of the encounters) multiplied by the desired delay of 90 seconds (which gives 7.2 NM).

For the linear feedback loop, the minimum distance ranges from 4 NM to 8.2 NM. Its average is 6.3 NM and the standard deviation is 1.1 NM. For the nonlinear feedback loop, the minimum distance ranges from 4 NM to 7.9 NM. Its average is 6.3 NM and the standard deviation is 1 NM.

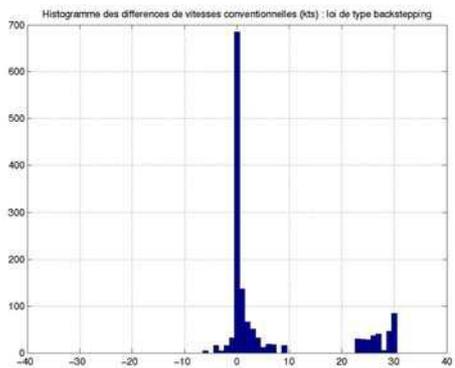
The number of encounters for which the minimum distance is between 3.5 and 4.5 NM is the

same for the linear and the nonlinear design (114 encounters), but the nonlinear design places fewer encounters in the set between 7.5 NM and 8.5 NM.

- The histogram of the difference between the conventional airspeed (CAS) of the leading and the trailing aircraft at the sequencing measurement point is represented on the following figures:



**Figure 12. Difference between the conventional airspeed of the two aircraft at the sequencing measurement point with the linear feedback loop**



**Figure 13. Difference between the conventional airspeed of the two aircraft at the sequencing measurement point with the nonlinear feedback loop**

For the linear feedback loop, there are 225 encounters for which the conventional airspeed (CAS) difference is +30 kts (i.e. the CAS of the following plane is 30 kts higher than the leading CAS at the sequencing measurement point), which indicates that the station keeping phase is not completely achieved (speed is not stabilized). For 355 encounters, the difference in speed is lower than 1.5 kts.

For the nonlinear feedback loop, there are only 84 encounters for which the conventional airspeed (CAS) difference is +30 kts. For 822 encounters, the

difference in speed is lower than 1.5 kts. This means that the time needed to achieve the station keeping phase is shorter with the nonlinear feedback loop, and consequently its operational acceptability would be greater.

## Conclusion

This paper deals with the design of a new autopilot mode dedicated to both merging at a specified meter fix and station keeping behind a designated aircraft. This is achieved through a feedback loop which controls speed and bank angle.

The main contributions of this paper consist firstly in a new nonlinear design of the feedback control loop and secondly in a statistical performance evaluation between a linear design and the proposed nonlinear design, namely a proportional/derivative design and the proposed backstepping design.

The statistical performance evaluation is based on a data base of 1408 merging encounters which are operationally realistic. For both designs the delay between the leading and the trailing aircraft measured at a sequencing measurement point matches the desired delay between the two aircraft. In addition, both designs allow for safe merging and station keeping guidance. Nevertheless, the time needed to achieve the station keeping phase is shorter with the nonlinear feedback loop compared to the linear feedback loop. This promotes the nonlinear design. Indeed, a touch of complexity in the design process allows for better performances in the relative guidance feedback loop which would in turn allow for better operational acceptability.

The results have been obtained by maintaining the trailing aircraft on its flight plan during the simulations: this is adapted to correct delays between the leading and the trailing aircraft of a few minutes (90 seconds in this evaluation). For higher delays to be compensated, it may be valuable to reinforce the effect of the relative guidance feedback loop by stretching the trajectory of the trailing aircraft through the generation of a reference trajectory. This deserves further refinements and validations of the proposed approach.

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### **Acknowledgements**

The authors wish to thank Christelle Pianetti, and Philippe Louyot from the Centre d'Études de la Navigation Aérienne for their helpful inputs and comments.

### **Keywords**

Airborne Separation Assistance System (ASAS), Sequencing and Merging Operations, Linear and Nonlinear Feedback Loop Design

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