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Modified Bezier Curve for 4D Reference Trajectory Definition under Flight Profile Constraint

Thierry Miquel*

Direction des Services de la Navigation Aérienne, Toulouse, FRANCE

Félix Mora-Camino†

Ecole Nationale de l'Aviation Civile and LAAS du CNRS, Toulouse, France

The task of establishing properly spaced landing sequences is quite demanding for air traffic controllers in heavy traffic conditions. Indeed, air traffic controllers combine two or more streams into a single stream before landing by means of radar vectoring and speed instructions. This high level task of sequencing aircraft is not currently communicated to the pilot. Instead, controller translate it into clearances to the pilot, typically radar vectoring and speed instructions. In this paper, the task of merging an aircraft over a specified meter fix is addressed through a novel 'Set Reference Path' procedure in which the air traffic controller may clear an aircraft to merge at a specified meter fix at a given time. This paper focuses on the definition of a reference path for time-based operations at meter fix. It includes path stretching operations, which occur when the aircraft is predicted to overfly too early a meter fix with respect to other traffic flow constraints. This paper presents a new approach to generate a reference path with length and endpoint constraints based on modified Bezier curves. Compared to reference trajectories based on straight lines and circle arcs, which are usual in the aviation community, the proposed approach allows for smooth control cues and avoids the scheduling between straight lines and circle arcs segments. The proposed design is followed by illustrative examples which show the effectiveness of the proposed approach.

I. Introduction

From the ICAO definition¹, ATS services include the prevention of collisions between aircraft and between aircraft on the ground and obstructions, the provision of advice to aircraft and information required for the safe and efficient conduct of flights and the achievement of an orderly and expeditious flow of air traffic. The overall goal of the R&D community has always been to improve Air Traffic Services (ATS) through a greater involvement of pilots in cooperation with air traffic controllers. For example, the Airborne Separation Assistance System (ASAS) concept was presented to ICAO in 2003 to take advantage of new airborne capabilities for surveillance². Indeed, ASAS is an airborne system that allows air traffic controllers to possibly delegate separation responsibility and transfers the corresponding separation tasks to the flight crew. ASAS allows the flight crew to maintain separation between their aircraft and one or more other aircraft, and provides information concerning the surrounding traffic. This system and associated concept basically address the ATS services dealing with the prevention of collisions and the provision of information on surrounding traffic to aircraft.

This paper addresses another aspect of ATS, namely the achievement of an orderly and expeditious flow of air traffic. Indeed, the task of establishing properly spaced landing sequences is quite demanding for air traffic controllers in heavy traffic conditions. More specifically, air traffic controllers combine two or more streams into a single stream before landing by means of radar vectoring and speed instructions. This high level task of sequencing aircraft is not currently communicated to the pilot. Instead, controller translate it into clearances to the pilot, typically radar vectoring and speed instructions. In this paper, the task of merging an aircraft over a specified meter fix is addressed through a novel 'Set Reference Path' procedure in which the air traffic controller may clear an

* PhD, Civil Aviation Design and Operation Engineer, Separation and Alerting Systems Unit, miquel@cena.fr

† Senior Researcher at LAAS du CNRS, Professor of Automatic Control and Avionics at Ecole Nationale de l'Aviation civile, Felix.MORA@enac.fr

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aircraft to merge at a specified meter fix at a given time. This procedure may be envisioned as the airborne counterpart of the ground based Arrival MANager (AMAN), which is a tactical controller assistance system enabling the computation of rendez-vous time at meter fix to meet the runway capacity and absorb the traffic. The time computed by the AMAN may then be used by the air traffic controller to ask the aircrew to overfly the meter fix at the desired time. This type of procedure is clearly in the scope of the 4D trajectory concept promoted by the European project SESAR³.

While keeping the controller in charge of Air Traffic Management (ATM), the procedure involves new avionics capabilities for merging operations, including path definition capabilities as well as tracking altitude, speed and heading cues. Indeed controllers remain responsible for making the traffic flow decisions; the change is that the controller would then communicate these decisions at a higher level to the pilot, e.g. ‘Be at Meter Fix ABCDE at 13:20:35’ rather than requiring the controller to calculate and communicate lower-level guidance instructions. The main expected benefit of this application is to increase capacity through the decrease of controller’s workload and to improve flight efficiency by more precise maneuvering from onboard capabilities.

As already mentioned, air traffic controller keeps the task of preventing collisions between aircraft. Thus, this kind of procedure is not an ASAS procedure. Nevertheless, it is also envisioned to combine this procedure with ASAS target trail mode in order to render possible a trailing aircraft to track the delayed path of the 4D managed aircraft, and thus maintain spacing between both aircraft, as showed in the following figure:

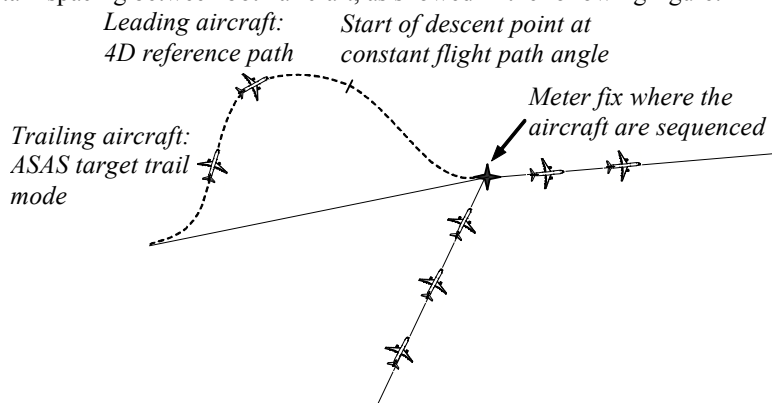


Fig. 1: combined ASAS target trail and 4D reference path operations

This paper focuses on the definition of a reference path for time-based operations at meter fix. It includes path stretching operations, which occur when the aircraft is predicted to overfly a meter fix with too early respect to other traffic flow constraints. The reference path definition problem consists in finding curves that satisfy constraints on length and on the positions and tangents at the two endpoints. Finding a smooth path with continuous curvature that can match arbitrary endpoint constraints and length constraint is nontrivial. Several techniques can be used, including geometric approaches^{4,5,6}, the use of optimal control^{7,8} as well as evolutionary algorithms⁹. In this paper, a geometric approach using modified Bezier curves is introduced.

The paper is organized as follows: in the next section, the parameterization of the reference trajectory is addressed. Then the definition of the reference trajectory for an airliner in order to obtain its arrival on a meter fix at a time chosen by air traffic control is addressed. This is done on the basis of modified Bezier curves which allows generating a path with length and endpoint constraints. The reference trajectory definition is followed by illustrative examples where level changes and wind are considered. Finally, conclusions on the effectiveness of the proposed approach are drawn.

II. Reference trajectory parameterization

A. Assumptions on flight profile

Most of Flight Crew Operating Manuals do not provide operating speed in terms of true airspeed, denoted V hereafter, but in terms of calibrated airspeed or Mach number. It is assumed in the following that the equivalent airspeed V_e , that is the calibrated airspeed corrected for the scale altitude error, is controlled by the aircrew. Denoting by $\sigma(h)$ the relative air density, which depends on altitude h , the relationship between true airspeed V and equivalent airspeed V_e is the following¹⁰:

$$\left\{ \begin{array}{l} V = \frac{V_e}{\sqrt{\sigma(h)}} \\ \sigma(h) = \frac{\rho(h)}{\rho(0)} \end{array} \right. \text{ where } \left\{ \begin{array}{l} \sqrt{\sigma(h)} = (1 + b \cdot h)^{-\lambda} \\ -\lambda = -\frac{1}{2} \cdot \left(\frac{g}{k_r \cdot R} + 1 \right) \approx \frac{4.2558}{2} \\ b = \frac{k_r}{T_0} \approx -\frac{0.0065}{288.15} m^{-1} \end{array} \right. \quad (1)$$

As far as the flight profile is concerned, it is assumed in the following that the 4D maneuver starts at flight level h_0 and is achieved at flight level h_1 . Flight level phase at h_0 is assumed to be followed by a descent phase at constant flight path angle, denoted γ_d , until flight level h_1 is reached. Furthermore it is assumed that the equivalent airspeed of the aircraft is constant and maintained to V_{e0} while the aircraft is level. Then the equivalent airspeed is assumed to linearly decrease towards V_{e1} during the descent phase. The following figure depicts the assumptions on the flight profile, where t_d denotes the duration of the descent phase, t_s the duration of the slow down phase where the equivalent airspeed decreases from V_{e0} to V_{e1} . In addition T denotes the requested instant at which the aircraft should be over the meter fix specified by the air traffic controller:

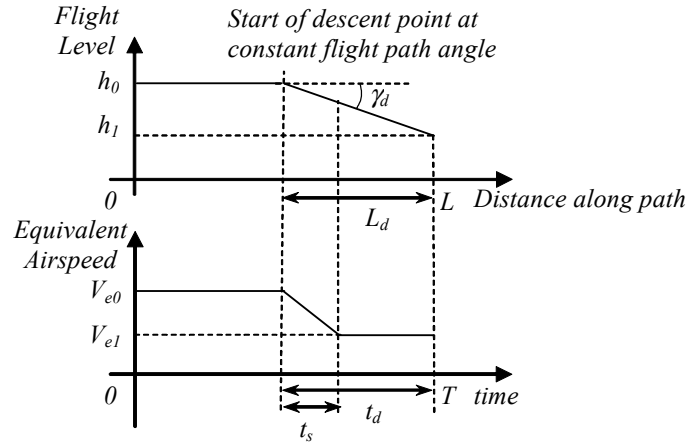


Fig. 2: assumption on flight profile

The rationale to assume a constant flight path angle during the descent comes from the longitudinal equation of motion. This equation is derived from Newton's second law of motion¹¹, where F is the thrust of the aircraft, D the drag, m the mass and g the gravitational acceleration:

$$m \cdot \frac{dV}{dt} = (F - D) - mg \cdot \sin(\gamma) \quad (2)$$

Introducing (1) and its time derivative in (2), we get:

$$\sin(\gamma) = \left(\frac{F - D}{mg} - \frac{\dot{V}_e}{g \cdot \sqrt{\sigma(h)}} \right) \cdot \frac{1}{(1 - f(h))} \quad \text{where } f(h) = V_e^2 \cdot \frac{d\sigma(h)/dh}{2 \cdot g \cdot \sigma^2(h)} \quad (3)$$

Calculations show that term $f(h)$ can be neglected compared to 1 when equivalent airspeed V_e and flight level h are set to typical values observed in approach control. Indeed, when flight level h varies from 0 to $FL100$ and for two values of equivalent airspeed, 100 kts and 250 kts, it can be seen that the maximum value of $f(h)$ is achieved at 250 kts and $FL100$, where the term $f(h)$ is about -0.117.

Consequently, assuming that acceleration of equivalent airspeed is *small* compared to gravitational acceleration g and that aircraft mass m and difference between thrust F and drag D remain constant, flight path angle γ can be assumed to remain constant during approach control.

Assuming that the requested duration T of the trajectory is known, the purpose of the following development is to express the value of duration t_d which enables to locate the start of descent instant and the value of the requested length L of the trajectory.

First, during the descent phase and duration t_s (see Fig. 2), the equivalent airspeed is assumed to have the following expression:

$$V_e(t) = V_{e0} + \frac{t}{t_s} \cdot (V_{e1} - V_{e0}) \quad (4)$$

In addition, the vertical speed of the aircraft is given by:

$$\frac{dh}{dt} = V(t) \cdot \sin(\gamma_d) \quad (5)$$

Combining equations (1), (4) and (5) lead to the following nonlinear first order differential equation:

$$\sqrt{\sigma(h)} \cdot dh = \left(V_{e0} + \frac{t}{t_s} \cdot (V_{e1} - V_{e0}) \right) \cdot \sin(\gamma_d) \cdot dt \quad (6)$$

Solving this differential equation under the assumption of standard atmosphere model¹¹ (below the Tropopause) leads to the expression of flight level h as a function of time t between instants t_d and $t_d + t_s$:

$$\frac{(1+b \cdot h(t))^{1-\lambda} - (1+b \cdot h_0)^{1-\lambda}}{b \cdot (1-\lambda)} = V_{e0} \cdot t \cdot \sin(\gamma_d) \cdot \left(1 + \frac{t}{2 \cdot t_s} \cdot \left(\frac{V_{e1}}{V_{e0}} - 1 \right) \right) \quad (7)$$

We then get the value of flight level $h(t_s)$:

$$h(t_s) = \frac{1}{b} \cdot \left(\left((1+b \cdot h_0)^{1-\lambda} + V_{e0} \cdot t_s \cdot \sin(\gamma_d) \cdot b \cdot (1-\lambda) \cdot \left(1 + \frac{1}{2} \cdot \left(\frac{V_{e1}}{V_{e0}} - 1 \right) \right) \right)^{\frac{1}{1-\lambda}} - 1 \right) \quad (8)$$

In addition, the time needed to go from flight level $h(t_s)$ to h_1 can be evaluated by an expression similar to (7) where V_{e0} is replaced by V_{e1} as far as during that segment the equivalent airspeed is constant and set to V_{e1} :

$$\frac{(1+b \cdot h_1)^{1-\lambda} - (1+b \cdot h(t_s))^{1-\lambda}}{b \cdot (1-\lambda)} = V_{e1} \cdot (t_d - t_s) \cdot \sin(\gamma_d) \quad (9)$$

Assuming that deceleration duration t_s , flight levels h_0 and h_1 , equivalent airspeed V_{e0} and V_{e1} are known, we get from the preceding equation the value of descent duration t_d as a function of $h(t_s)$, which is available through (8):

$$t_d = t_s + \frac{1}{V_{e1} \cdot \sin(\gamma_d)} \cdot \left(\frac{(1+b \cdot h_1)^{1-\lambda} - (1+b \cdot h(t_s))^{1-\lambda}}{b \cdot (1-\lambda)} \right) \quad (10)$$

Finally, assuming that the requested duration of flight T is known and greater than duration of the descent phase t_d , the required length L of the trajectory is found to be:

$$L = V(h_0) \cdot (T - t_d) + L_d \quad (11)$$

Where the distance L_d which is flown during the descent phase has the following expression:

$$L_d = \left| \frac{h_1 - h_0}{\sin(\gamma_d)} \right| \quad (12)$$

B. Trajectory parameterization

Assuming that Earth is flat and non-rotating, it may be considered as an inertial frame. The kinematics equations describing the aircraft motion are recalled hereafter, where x , y and h refer to Euclidian position, no subscript refers to the airframe and subscript g to earth reference frame. In the following, V denotes the airspeed of the aircraft, γ its flight path angle and ψ its heading. In addition ψ_w denotes the direction *from* where the (horizontal) wind is blowing and V_w the constant wind velocity, and no vertical wind component is assumed:

$$\begin{cases} \dot{x}_g(t) = \dot{x}(t) + V_w \cdot \cos(\psi_w - \pi) \\ \dot{y}_g(t) = \dot{y}(t) + V_w \cdot \sin(\psi_w - \pi) \\ \dot{h}_g(t) = \dot{h}(t) \end{cases} \quad (13)$$

Where

$$\begin{cases} \dot{x}(t) = V(t) \cdot \cos(\gamma(t)) \cdot \cos(\psi(t)) \\ \dot{y}(t) = V(t) \cdot \cos(\gamma(t)) \cdot \sin(\psi(t)) \\ \dot{h}(t) = V(t) \cdot \sin(\gamma(t)) \end{cases} \quad (14)$$

Integrating the preceding set of equations leads to expression of the ground based aircraft coordinates $x_g(t)$, $y_g(t)$ and $h_g(t)$ as a function of the air based aircraft coordinates $x(t)$, $y(t)$ and $h(t)$:

$$\begin{cases} x_g(t) = x_g(0) + x(t) + V_w \cdot t \cdot \cos(\psi_w - \pi) \\ y_g(t) = y_g(0) + y(t) + V_w \cdot t \cdot \sin(\psi_w - \pi) \\ h_g(t) = h_g(0) + h(t) \end{cases} \quad \text{where} \quad \begin{cases} x(t) = \int_0^t \dot{x}(u) \cdot du \\ y(t) = \int_0^t \dot{y}(u) \cdot du \\ h(t) = \int_0^t \dot{h}(u) \cdot du \end{cases} \quad (15)$$

As described in the introduction section, the envisioned operational procedure assumes that the air traffic control requests the aircrew to be over a given meter fix at a given time T and at the given flight level h_I . The aircrew will comply with that request by adjusting the length of the trajectory under constrained flight level and equivalent airspeed. Indeed, it is assumed that airspeed of the aircraft is indirectly known and imposed for example by Flight Crew Operating Manual. So, the reference trajectory definition problem consists in finding a mapping $t \rightarrow \mathbf{P}(t) = [x(t), y(t), h(t)]^T$ such that constraints on the positions and tangents at the two endpoints at time $t = 0$ and $t = T$ are satisfied. Furthermore, the mapping $t \rightarrow \mathbf{P}(t) = [x(t), y(t), h(t)]^T$ shall also satisfy speed constraints.

In the following the aircraft trajectory is described as mapping from a dimensionless interval to R^3 . More precisely, let $\mathbf{P}(\tau) \rightarrow R^3$ be the aircraft trajectory, where dimensionless parameter τ is taken within the interval $[0, 1]$. The definition of dimensionless parameter τ may either involve time or arc length. In order to alleviate the mapping to be found from the speed constraint, parameter τ has been chosen to be proportional to the arc length $s(t)$ but not to time t . Consequently, the constraint on speed profile is changed into a constraint on the length of the trajectory. More specifically, dimensionless parameter τ is defined hereafter where T is the prescribed duration of the maneuver and L the length of the trajectory when the maneuver is completed:

$$\tau(t) = \frac{s(t)}{L} \quad \text{where} \quad \begin{cases} s(0) \doteq 0 \\ s(T) \doteq L \end{cases} \quad (16)$$

The rationale for this parameterization comes from the definition of the airspeed which is the time derivative of the arc length, that is:

$$V(t) = \frac{ds(t)}{dt} \quad (17)$$

In addition, the time derivative of parameter τ can be deduced from (16) and (17) by using the derivative chain rule:

$$\frac{d\tau(t)}{dt} = \frac{d\tau(s)}{ds} \cdot \frac{ds(t)}{dt} = \frac{V(t)}{L} \quad (18)$$

When using the previous relationship with (14), we get:

$$\begin{cases} \frac{d}{d\tau} x(\tau) = L \cdot \cos(\gamma(\tau)) \cdot \cos(\psi(\tau)) \\ \frac{d}{d\tau} y(\tau) = L \cdot \cos(\gamma(\tau)) \cdot \sin(\psi(\tau)) \\ \frac{d}{d\tau} h(\tau) = L \cdot \sin(\gamma(\tau)) \end{cases} \quad (19)$$

It is worth noticing that airspeed $V(t)$ simplifies in the previous equations. Consequently trajectory $\mathbf{P}(\tau) = [x(\tau), y(\tau), h(\tau)]^T$ is now independent from airspeed: this justifies to choose parameter τ proportional to the arc length. The two endpoints of the trajectory are denoted respectively $\mathbf{P}(0)$ and $\mathbf{P}(1)$, where $\mathbf{P}(0)$ is the starting point of the trajectory and $\mathbf{P}(1)$ is the ending point. The Cartesian expression of trajectory $\mathbf{P}(\tau)$ is:

$$\mathbf{P}(\tau) = \begin{bmatrix} x(\tau) \\ y(\tau) \\ h(\tau) \end{bmatrix} \quad (20)$$

As far as initial and final flight path angle and heading are assumed to be known, trajectory $\mathbf{P}(\tau)$ shall satisfy the following endpoint constraints, where γ_d stands for the final flight path angle and ψ_0 and ψ_I stand for the initial and final heading:

$$\begin{cases} \frac{d}{d\tau}x(0) = L \cdot \cos(\psi_0) \\ \frac{d}{d\tau}y(0) = L \cdot \sin(\psi_0) \\ \frac{d}{d\tau}h(0) = 0 \end{cases} \quad \text{where} \quad \begin{cases} \frac{d}{d\tau}x(1) = L \cdot \cos(\psi_1) \cdot \cos(\gamma_d) \\ \frac{d}{d\tau}y(1) = L \cdot \sin(\psi_1) \cdot \cos(\gamma_d) \\ \frac{d}{d\tau}h(1) = L \cdot \sin(\gamma_d) \end{cases} \quad (21)$$

In addition, flight level $h(\tau)$ is set as follows where $\Gamma(x)$ stands for the Heaviside step function (its value is 1 if $x > 0$, and 0 otherwise) in order to satisfy the requested vertical flight profile:

$$h(\tau) = h_0 + (h_1 - h_0) \cdot \left(\frac{\tau - \tau_d}{1 - \tau_d} \right) \cdot \Gamma(\tau - \tau_d) \quad \text{where} \quad \tau_d = 1 - \left| \frac{h_1 - h_0}{L \cdot \sin(\gamma_d)} \right| \quad (22)$$

The preceding relationship completely defines the vertical profile of the aircraft. The purpose of the next section is to define the lateral reference trajectory of the aircraft, that is the expression of horizontal coordinates $x(\tau)$ and $y(\tau)$.

III. Reference trajectory Definition

A. Bezier curve

The objective of the reference trajectory definition consists of generating a smooth trajectory by joining two distinct configurations, the oriented starting and ending points, with a constraint on the length at which the ending point is reached. In this section, vector $[x(\tau), y(\tau)]^T$ is assumed to follow a Bezier curve of dimension 2:

$$\begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} = \sum_{i=0}^3 \binom{3}{i} \cdot \tau^i \cdot (1-\tau)^{3-i} \cdot \mathbf{P}_{i/3} \quad (23)$$

Points $\mathbf{P}_{0/3}$ and $\mathbf{P}_{3/3}$ are respectively the (given) starting and ending points of the trajectory. Points $\mathbf{P}_{i/3}$, $i \in \{1,2\}$, are used as parameterization points of the trajectory. Points $\mathbf{P}_{1/3}$ and $\mathbf{P}_{2/3}$ are used to direct the initial and final orientation of the trajectory according to the initial and final headings. The following figure presents a possible positioning of the parameterization points $\mathbf{P}_{i/3}$, where ψ_0 and ψ_1 stands for the initial and final heading, and where ψ_2 stands for the direction of the vector $\mathbf{P}_{0/3}\mathbf{P}_{3/3}$:

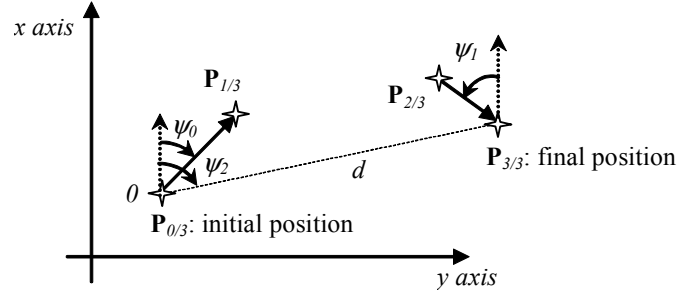


Fig. 3: Parameterization of Bezier curve

Without loss of generality, points $\mathbf{P}_{0/3}$ and $\mathbf{P}_{3/3}$ are set as follows, where d is the distance between initial and final positions:

$$\begin{cases} \mathbf{P}_{0/3} \hat{=} \begin{bmatrix} 0 \\ 0 \end{bmatrix} \\ \mathbf{P}_{3/3} - \mathbf{P}_{0/3} \hat{=} d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} \end{cases} \quad (24)$$

Then, the first derivative of vector $[x(\tau), y(\tau)]^T$ is given by:

$$\frac{d}{d\tau} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} = 3 \cdot (\tau - 1) \cdot (3\tau - 1) \cdot \mathbf{P}_{1/3} + 3 \cdot \tau \cdot (2 - 3\tau) \cdot \mathbf{P}_{2/3} + 3 \cdot \tau^2 \cdot d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} \quad (25)$$

If we set points static $\mathbf{P}_{1/3}$ and $\mathbf{P}_{2/3}$ such that endpoint constraints (21) are satisfied, it can be seen that no degree of freedom remains to satisfy the constraint that the length of the trajectory shall be equal to L . In order to alleviate this issue, points $\mathbf{P}_{1/3}$ and $\mathbf{P}_{2/3}$ have been defined as a function of parameter τ .

B. Modified Bezier curve

Compared to classical Bezier curve where points $\mathbf{P}_{i/3}$, $i \in \{0,1,2,3\}$ do not evolve with parameter τ , a new approach is developed in this paper where points $\mathbf{P}_{1/3}$ and $\mathbf{P}_{2/3}$ are a function of parameter τ . First, relationship (23) is expanded as follows:

$$\begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} = (1-\tau)^3 \cdot \mathbf{P}_{0/3} + 3 \cdot \tau \cdot (1-\tau)^2 \cdot \mathbf{P}_{1/3}(\tau) + 3 \cdot \tau^2 \cdot (1-\tau) \cdot \mathbf{P}_{2/3}(\tau) + \tau^3 \cdot \mathbf{P}_{3/3} \quad (26)$$

Then, the following parameterization of points $\mathbf{P}_{1/3}$ and $\mathbf{P}_{2/3}$ is introduced, where d is the Euclidian distance between starting point $\mathbf{P}_{0/3}$ and final point $\mathbf{P}_{3/3}$, L is the desired length of the trajectory and where λ_0 and λ_l are constant parameters to be set:

$$\begin{cases} \mathbf{P}_{1/3}(\tau) \hat{=} \mathbf{P}_{0/3} + \left(\lambda_0 \cdot \tau + \frac{1}{3} \right) \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} \\ \mathbf{P}_{2/3}(\tau) \hat{=} \mathbf{P}_{3/3} + \left(\lambda_l \cdot (\tau-1) - \frac{1}{3} \right) \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \cdot \cos(\gamma_d) \\ \sin(\psi_1) \cdot \cos(\gamma_d) \end{bmatrix} \end{cases} \quad (27)$$

Using parameterization (27) into the general expression of modified Bezier curve (26) leads to the following expression:

$$\begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} = 3 \cdot \tau \cdot (1-\tau)^2 \cdot \mathbf{P}_{1/3}(\tau) + 3 \cdot \tau^2 \cdot (1-\tau) \cdot \mathbf{P}_{2/3}(\tau) + \tau^3 \cdot d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} \quad (28)$$

The first and second derivative of $x(\tau)$ and $y(\tau)$ are the following:

$$\frac{d}{d\tau} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} = 3 \cdot (\tau-1) \cdot (3\tau-1) \cdot \mathbf{P}_{1/3}(\tau) + 3 \cdot \tau \cdot (2-3\tau) \cdot \mathbf{P}_{2/3}(\tau) + 3 \cdot \tau^2 \cdot d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} \quad (29)$$

$$\begin{aligned} &+ 3 \cdot \tau \cdot (1-\tau)^2 \cdot \lambda_0 \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} + 3 \cdot \tau^2 \cdot (1-\tau) \cdot \lambda_l \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \cdot \cos(\gamma_d) \\ \sin(\psi_1) \cdot \cos(\gamma_d) \end{bmatrix} \\ \frac{d^2}{d\tau^2} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} &= 3 \cdot (6\tau-4) \cdot \mathbf{P}_{1/3}(\tau) + 3 \cdot (2-6\tau) \cdot \mathbf{P}_{2/3}(\tau) + 6 \cdot \tau \cdot d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} \quad (30) \\ &+ 3 \cdot (\tau-1) \cdot (3\tau-1) \cdot \lambda_0 \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} + 3 \cdot \tau \cdot (2-3\tau) \cdot \lambda_l \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \cdot \cos(\gamma_d) \\ \sin(\psi_1) \cdot \cos(\gamma_d) \end{bmatrix} \end{aligned}$$

We get the following values at the beginning and at the end of the trajectory, which satisfy endpoint constraints (21):

$$\begin{bmatrix} x(0) \\ y(0) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} x(1) \\ y(1) \end{bmatrix} = d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} \quad (31)$$

$$\begin{bmatrix} \frac{dx}{d\tau}(0) \\ \frac{dy}{d\tau}(0) \end{bmatrix} = 3 \cdot \mathbf{P}_{1/3}(0) = L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} \frac{dx}{d\tau}(1) \\ \frac{dy}{d\tau}(1) \end{bmatrix} = -3 \cdot \mathbf{P}_{2/3}(1) + 3 \cdot d \cdot \begin{bmatrix} \cos(\psi_2) \\ \sin(\psi_2) \end{bmatrix} = L \cdot \begin{bmatrix} \cos(\psi_1) \cdot \cos(\gamma_d) \\ \sin(\psi_1) \cdot \cos(\gamma_d) \end{bmatrix} \quad (32)$$

C. Optimization problem

Now that a generic shape of the trajectory has been defined, parameters λ_0 and λ_l have to be set to satisfy length constraint. As far as we have two parameters to be set, parameters λ_0 and λ_l will be set to satisfy the length trajectory constraint while minimizing the mean square of curvature of the trajectory. The rationale for the minimization of the mean square of curvature is to provide as best as possible a flyable trajectory.

The length l of the trajectory when parameter τ varies from 0 to 1 is defined as a function of parameters λ_0 and λ_l by:

$$l(\lambda_0, \lambda_l) = \int_0^1 \sqrt{\frac{d\mathbf{P}(\tau)^T}{d\tau} \cdot \frac{d\mathbf{P}(\tau)}{d\tau}} \cdot d\tau \quad (33)$$

The curvature $K(s)$ of the trajectory $\mathbf{P}(\tau)$ is defined by the following relationship¹², where s represents the arc length of the trajectory:

$$K(s) = \sqrt{\left(\frac{d^2\mathbf{P}(s)}{ds^2} \right)^T \cdot \frac{d^2\mathbf{P}(s)}{ds^2}} \quad (34)$$

In the following, k is used to denote the mean square of curvature of the trajectory $\mathbf{P}(\tau)$ when parameter τ varies from 0 to 1. Using (16) and the derivative chain rule, this can be computed as a function of parameters λ_0 and λ_1 as follows:

$$k(\lambda_0, \lambda_1) \triangleq \frac{1}{L} \cdot \int_0^L K^2(s) \cdot ds = \frac{1}{L^4} \cdot \int_0^1 \left(\frac{d^2 \mathbf{P}(\tau)}{d\tau^2} \right)^T \cdot \frac{d^2 \mathbf{P}(\tau)}{d\tau^2} \cdot d\tau \quad (35)$$

Parameters λ_0 and λ_1 will be computed so that the mean square of curvature is minimized subject to the constraint that the horizontal trajectory length is L_h .

$$\min(k(\lambda_0, \lambda_1)) \quad s.t. \quad l(\lambda_0, \lambda_1) = L_h \quad (36)$$

Horizontal trajectory length is L_h is defined from (11) by:

$$L_h = V(h_0) \cdot (T - t_d) + L_d \cdot \cos(\gamma_d) \quad (37)$$

Solution of this optimization problem can be found through classical theory of minima and maxima¹³. First, an augmented function H is formed by using a Lagrange multiplier μ :

$$H(\lambda_0, \lambda_1) = k(\lambda_0, \lambda_1) + \mu \cdot (l(\lambda_0, \lambda_1) - L_h) \quad (38)$$

Then, stationary points of H are required to satisfy:

$$\begin{cases} \frac{\partial H}{\partial \lambda_0} = \frac{\partial k(\lambda_0, \lambda_1)}{\partial \lambda_0} + \mu \cdot \frac{\partial l(\lambda_0, \lambda_1)}{\partial \lambda_0} = 0 \\ \frac{\partial H}{\partial \lambda_1} = \frac{\partial k(\lambda_0, \lambda_1)}{\partial \lambda_1} + \mu \cdot \frac{\partial l(\lambda_0, \lambda_1)}{\partial \lambda_1} = 0 \\ l(\lambda_0, \lambda_1) - L_h = 0 \end{cases} \quad (39)$$

The two first equations can be combined in order to be solved in the Lagrange multiplier μ . Thus, the preceding set of three equations can be reduced to a set of two equations where Lagrange multiplier μ do not appear:

$$\begin{cases} \frac{\partial l(\lambda_0, \lambda_1)}{\partial \lambda_0} \cdot \frac{\partial k(\lambda_0, \lambda_1)}{\partial \lambda_1} - \frac{\partial l(\lambda_0, \lambda_1)}{\partial \lambda_1} \cdot \frac{\partial k(\lambda_0, \lambda_1)}{\partial \lambda_0} = 0 \\ l(\lambda_0, \lambda_1) - L_h = 0 \end{cases} \quad (40)$$

We get from (33) and (35) the following expressions for the partial derivatives:

$$\frac{\partial l(\lambda_0, \lambda_1)}{\partial \lambda_0} = \int_0^1 \frac{\left(\frac{\partial}{\partial \lambda_0} \left(\frac{d\mathbf{P}(\tau)}{d\tau} \right) \right)^T \cdot \frac{d\mathbf{P}(\tau)}{d\tau}}{\sqrt{\frac{d\mathbf{P}(\tau)^T}{d\tau} \cdot \frac{d\mathbf{P}(\tau)}{d\tau}}} \cdot d\tau \quad \text{and} \quad \frac{\partial l(\lambda_0, \lambda_1)}{\partial \lambda_1} = \int_0^1 \frac{\left(\frac{\partial}{\partial \lambda_1} \left(\frac{d\mathbf{P}(\tau)}{d\tau} \right) \right)^T \cdot \frac{d\mathbf{P}(\tau)}{d\tau}}{\sqrt{\frac{d\mathbf{P}(\tau)^T}{d\tau} \cdot \frac{d\mathbf{P}(\tau)}{d\tau}}} \cdot d\tau \quad (41)$$

$$\frac{\partial k(\lambda_0, \lambda_1)}{\partial \lambda_0} = \frac{2}{L^4} \cdot \int_0^1 \left(\frac{\partial}{\partial \lambda_0} \left(\frac{d^2 \mathbf{P}(\tau)}{d\tau^2} \right) \right)^T \cdot \frac{d^2 \mathbf{P}(\tau)}{d\tau^2} \cdot d\tau \quad \text{and} \quad \frac{\partial k(\lambda_0, \lambda_1)}{\partial \lambda_1} = \frac{2}{L^4} \cdot \int_0^1 \left(\frac{\partial}{\partial \lambda_1} \left(\frac{d^2 \mathbf{P}(\tau)}{d\tau^2} \right) \right)^T \cdot \frac{d^2 \mathbf{P}(\tau)}{d\tau^2} \cdot d\tau \quad (42)$$

In addition, we have from (27) and (29) the following expressions:

$$\begin{aligned} \frac{\partial}{\partial \lambda_0} \left(\frac{d}{d\tau} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= 3 \cdot (\tau - 1) \cdot (3\tau - 1) \cdot \frac{\partial}{\partial \lambda_0} \mathbf{P}_{1/3}(\tau) + 3 \cdot \tau \cdot (1 - \tau)^2 \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} \\ \Leftrightarrow \frac{\partial}{\partial \lambda_0} \left(\frac{d}{d\tau} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= 6 \cdot \tau \cdot (\tau - 1) \cdot (2\tau - 1) \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} \end{aligned} \quad (43)$$

And

$$\begin{aligned} \frac{\partial}{\partial \lambda_1} \left(\frac{d}{d\tau} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= 3 \cdot \tau \cdot (2 - 3\tau) \cdot \frac{\partial}{\partial \lambda_1} \mathbf{P}_{2/3}(\tau) + 3 \cdot \tau^2 \cdot (1 - \tau) \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \\ \sin(\psi_1) \end{bmatrix} \\ \Leftrightarrow \frac{\partial}{\partial \lambda_1} \left(\frac{d}{d\tau} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= -6 \cdot \tau \cdot (\tau - 1) \cdot (2\tau - 1) \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \\ \sin(\psi_1) \end{bmatrix} \end{aligned} \quad (44)$$

Similarly, we get from (27) and (30) the following expressions:

$$\begin{aligned} \frac{\partial}{\partial \lambda_0} \left(\frac{d^2}{d\tau^2} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= 3 \cdot (6\tau - 4) \cdot \frac{\partial}{\partial \lambda_0} \mathbf{P}_{1/3}(\tau) + 3 \cdot (\tau - 1) \cdot (3\tau - 1) \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} \\ \Leftrightarrow \frac{\partial}{\partial \lambda_0} \left(\frac{d^2}{d\tau^2} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= 3 \cdot (9\tau^2 - 8\tau + 1) \cdot L \cdot \begin{bmatrix} \cos(\psi_0) \\ \sin(\psi_0) \end{bmatrix} \end{aligned} \quad (45)$$

And

$$\begin{aligned} \frac{\partial}{\partial \lambda_1} \left(\frac{d^2}{d\tau^2} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= 3 \cdot (2 - 6\tau) \cdot \frac{\partial}{\partial \lambda_1} \mathbf{P}_{2/3}(\tau) + 3 \cdot \tau \cdot (2 - 3\tau) \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \\ \sin(\psi_1) \end{bmatrix} \\ \Leftrightarrow \frac{\partial}{\partial \lambda_1} \left(\frac{d^2}{d\tau^2} \begin{bmatrix} x(\tau) \\ y(\tau) \end{bmatrix} \right) &= -3 \cdot (9\tau^2 - 10\tau + 2) \cdot L \cdot \begin{bmatrix} \cos(\psi_1) \\ \sin(\psi_1) \end{bmatrix} \end{aligned} \quad (46)$$

As far as the solving the set equations (40) with expressions (41) - (46) is quite involved, numerical computation is used to solve this set of equations of the form:

$$\begin{cases} f_1(\lambda_0, \lambda_1) = 0 \\ f_2(\lambda_0, \lambda_1) = 0 \end{cases} \quad (47)$$

D. Procedure to build aircraft guidance cues

Knowing the desired duration of the trajectory, denoted T , as well as the initial and final equivalent airspeed and flight level of the aircraft (see Fig. 2), the methodology to build the reference trajectory to be flown by the aircraft is the following:

- Firstly, compute the desired length of the trajectory, L , as well as the duration of the descent phase, denoted t_d , using relationships (8), (10), (11) and (12). The value of duration t_d sets the start of descent instant and the longitudinal profile of the aircraft. As far as aircraft guidance cues are concerned, the scheduling of the longitudinal autopilot modes is the following: select flight level h_0 and airspeed V_{e0} ; then, when the start of descent point is reached, select flight path angle γ_d and airspeed V_{e1} .

- Secondly, define the initial and final positions of the air based coordinates of the aircraft (see Fig. 3) from the ground based endpoints constraints ($x_g(0)$, $y_g(0)$, $x_g(T)$ and $y_g(T)$) by using (15) and the knowledge of wind speed and direction *from where* wind is blowing, V_w and ψ_w respectively. In addition, use (13) and speed triangle inversion¹⁴ to set the initial and final headings, ψ_0 and ψ_1 respectively, of the air based reference trajectory from the constraints of initial and final ground based orientation χ :

$$\begin{cases} \mathbf{P}_{0/3} = \begin{bmatrix} x_g(0) \\ y_g(0) \end{bmatrix} \\ \mathbf{P}_{3/3} = \begin{bmatrix} x(T) \\ y(T) \end{bmatrix} = \begin{bmatrix} x_g(T) - V_w \cdot T \cdot \cos(\psi_w - \pi) \\ y_g(T) - V_w \cdot T \cdot \sin(\psi_w - \pi) \end{bmatrix} \end{cases} \quad (48)$$

$$\psi = \chi - \arcsin\left(\frac{V_w \cdot \sin(\chi - \psi_w)}{V \cdot \cos(\gamma)}\right) \quad (49)$$

- Finally solve the parameter optimization problem described in section III-C and compute the lateral reference trajectory $[x(\tau), y(\tau)]^T$. As far as guidance cues are concerned, reference heading ψ_r is computed from (19) as:

$$\psi_r(\tau) = \arctan\left(\frac{dy(\tau)/d\tau}{dx(\tau)/d\tau}\right) \quad (50)$$

In order to visualize the ground path $[x_g(\tau), y_g(\tau)]^T$, the following differential equations (see (14) and (18)) have to be solved, knowing that the airspeed profile $V_e(t)$ is known as soon as descent duration t_d is computed:

$$\begin{cases} \frac{d}{dt} \tau(t) = \frac{V_e(t)}{L \cdot \sqrt{\sigma(h)}} \\ \frac{d}{dt} h(t) = \frac{V_e(t)}{\sqrt{\sigma(h)}} \cdot \sin(\gamma_d) \cdot \Gamma(t - (T - t_d)) \end{cases} \quad \text{with} \quad \begin{cases} \tau(0) = 0 \\ h(0) = h_0 \end{cases} \quad (51)$$

Then, as far as the bijective relationship between parameter τ is known as a function of time t , the ground path is simply obtained by integrating (13):

$$\begin{cases} x_g(\tau) = x(\tau) + L \cdot W \cdot \cos(\psi_w - \pi) \cdot \int_0^\tau \frac{du}{V(u)} = x(\tau) + W \cdot t(\tau) \cdot \cos(\psi_w - \pi) \\ y_g(\tau) = y(\tau) + L \cdot W \cdot \sin(\psi_w - \pi) \cdot \int_0^\tau \frac{du}{V(u)} = y(\tau) + W \cdot t(\tau) \cdot \sin(\psi_w - \pi) \end{cases} \quad (52)$$

As far as the flyability of the reference trajectory is concerned, the reference bank angle ϕ_r can be evaluated by:

$$V \cdot \frac{d\psi(t)}{dt} = g \cdot \tan(\phi_r) \Rightarrow \begin{cases} \phi_r = \arctan\left(\frac{V^2}{g \cdot L} \cdot \frac{d\psi_r(\tau)}{d\tau}\right) \\ \frac{d\psi_r(\tau)}{d\tau} = \frac{y''(\tau) \cdot x'(\tau) - y'(\tau) \cdot x''(\tau)}{(x'(\tau))^2 + (y'(\tau))^2} \end{cases} \quad (53)$$

IV. Illustrative examples

The scenario which is used hereafter is built around real life meter fixes of an air navigation procedure to reach Paris Charles De Gaulle airport in France, runway 09R. We assume that an Airbus A330-300 is asked for a 4D operation during its initial approach. More precisely, we will assume that the aircraft is at FL100 with an equivalent airspeed of 250 kts and a course of 36 degrees when she overflies meter fix SUBOX. She is then required to achieve the Initial Fix at 3000 ft with a course of 87 degrees and airspeed of 170 kts. Assuming that meter fix is at the origin of the frame, the case study scenario is illustrated on the following figure:

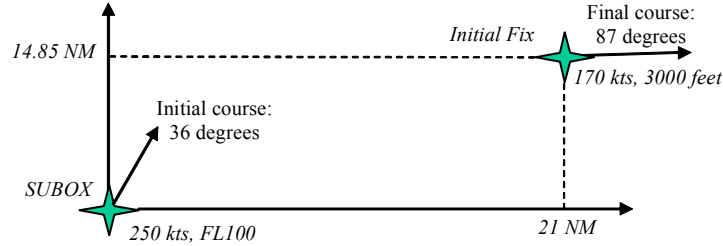


Fig. 4: case study scenario

Flight path angle γ_0 has been set to -3 degrees, whereas deceleration time t_s from 250 kts to 170 kts has been set to 80 sec (which corresponds to a deceleration of -1 kts per second). For this flight profile, the duration of the descent phase, t_d , has been found to be 404 sec (see (10)).

In the following table, four scenarios are presented: the inputs are the requested duration of the trajectory, denoted T , the wind speed V_w and the direction from where the wind is blowing, ψ_w ; the outputs are the parameters which enables to set the modified Bezier curves, namely the trajectory length L with respect to the airframe as well as parameters λ_0 and λ_1 :

Scenario	Requested duration T Wind speed V_w and direction ψ_w	Trajectory length with respect to the airframe L	Parameters λ_0 and λ_1
1	$T = 510 \text{ sec}$ $V_w = 0$	30.3 NM	$\lambda_0 = 0.323625$ $\lambda_1 = 1.127037$
2	$T = 600 \text{ sec}$ $V_w = 0$	37.6 NM	$\lambda_0 = 0.403293$ $\lambda_1 = 1.786681$
3	$T = 510 \text{ sec}$ $V_w = 30 \text{ kts}, \psi_w = 90 \text{ degrees}$	30.3 NM	$\lambda_0 = 0.011309$ $\lambda_1 = -0.098885$
4	$T = 600 \text{ sec}$ $V_w = 30 \text{ kts}, \psi_w = 90 \text{ degrees}$	37.6 NM	$\lambda_0 = 0.291503$ $\lambda_1 = 1.382552$

Fig. 5: scenario definition and parameters of the modified Bezier curves

The following figures illustrate the ground path achieved for each scenario. This is the kind of path that air traffic controllers may see on their working positions:

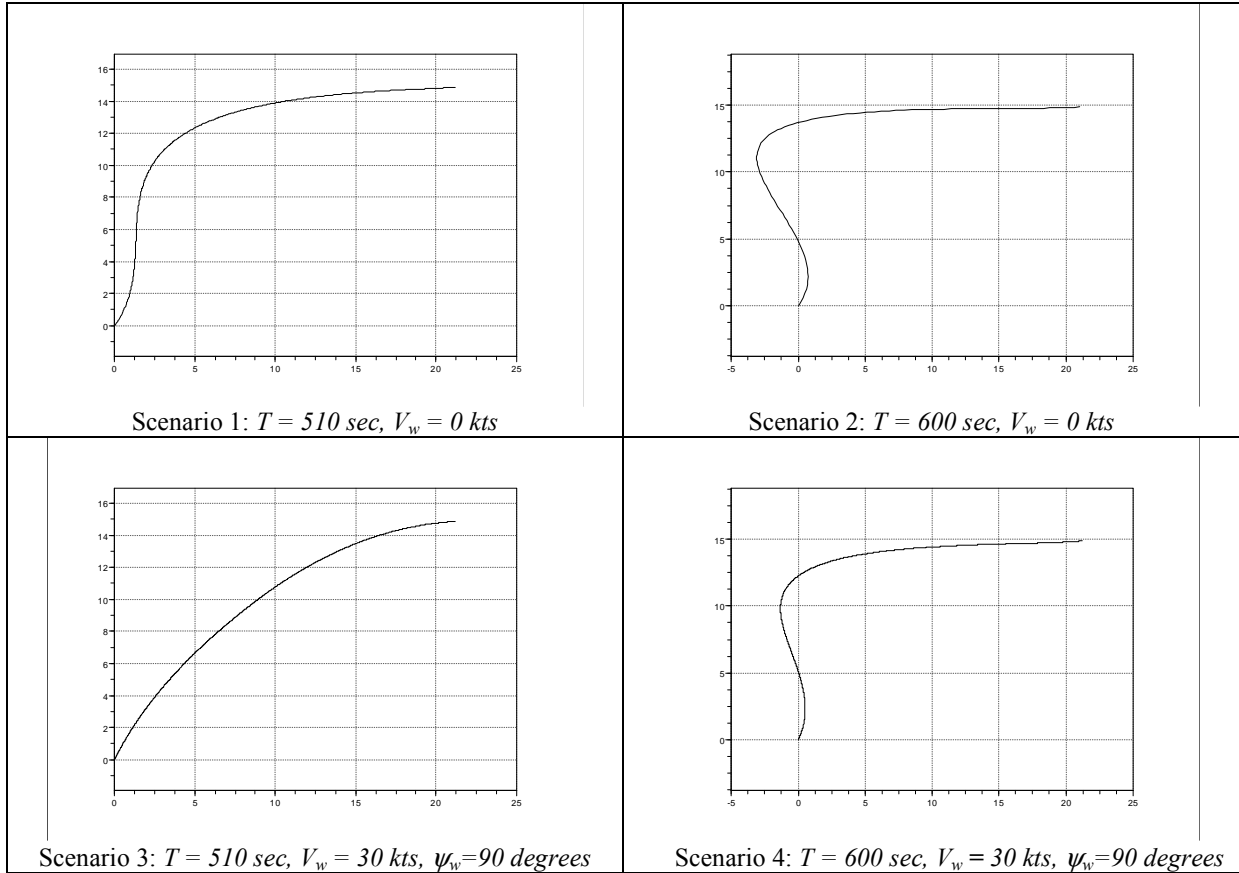


Fig. 6: ground path, Euclidian coordinates in NM

It can be seen from the previous figures that, compared to reference trajectories based on straight lines and circle arcs, which are usual in the aviation community, the proposed approach allows for smooth continuous control cues and avoids the scheduling between straight lines and circle arcs segments.

V. Conclusion

In this paper, the design of a new FMS function dedicated to reference path definition for 4D operation has been considered. This new function aims at achieving a specified delay between commercial aircraft at a specified meter fix. This envisioned new capability onboard commercial aircraft provides new perspectives to potentially increase air traffic control efficiency. It could be seen as the airborne counterpart of the ground based arrival manager (AMAN).

The reference path definition is based on modified Bezier curves to generate a path with length and endpoint constraints. The modified Bezier curve is parameterized with a linear function of the arc length, which allows designing the reference trajectory without considering airspeed constraints.

Compared to reference trajectories based on straight lines and circle arcs, which are usual in the aviation community, the proposed approach allows for smooth control cues and avoids the scheduling between straight lines and circle arcs segments.

Simulation results illustrate the effectiveness of the proposed design. Nevertheless, the proposed design is quite demanding in terms of (off line) computational efforts, and improvements may be needed to incorporate it in new FMS functionalities. The tracking of the reference trajectory has also to be addressed. Finally, additional studies in terms of operational scenarios are needed in order to refine and further validate the proposed design.

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