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Probability of Secondary Code Acquisition for Multi-Component GNSS Signals

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Abstract— The number of transmitted GNSS (Global Navigation Satellite Systems) signals has increased significantly with Galileo, Compass and QZSS constellations' ongoing deployment, GLONASS constellation maintenance and the introduction of new GPS signals. All the future GNSS civil signals are composed of two components: one being the pilot component which contains known secondary codes. In order to avoid fully exploit secondary code properties and the bit transition problem on the pilot component allowing long coherent integration for a better tracking, it is necessary to acquire the secondary code. This paper presents a mathematical model that determines the probability of correct acquisition of the secondary code once the spreading code has been acquired. The second point of the paper is the presentation of experimental results which provides some interesting results in terms of secondary code acquisition. The first one is the probability of secondary code acquisition when it is only read once. The second one corresponds to the required time to acquire the secondary code with a high probability for a given C/N_0 . These results, provided for four GNSS signals (GPS L1C, GPS L5, Galileo E1 OS and Galileo E5a/b) permit to compare the U.S GNSS with the European GNSS for several L band frequencies (L1 and L5).

Keywords—Pilot component, Secondary code, Autocorrelation, Acquisition

I. INTRODUCTION

Before having a closer look into the detailed secondary code autocorrelation study, a general view on the secondary codes uses will start the paper.

GNSS signals are composed of a carrier which carries a navigation message and a spreading code sequence which permits to share a band of frequencies between several GNSS satellites signals (in the same constellation or not), via Code Division Multiple access (CDMA). The new generation of GPS signals and Galileo signals are composed of two components: the data component, which is modulated by a data message and the pilot component, which is dataless but contains a known secondary code.

The pilot component is introduced to avoid the data bit transition problem on the data component. Indeed, the pilot component is fully known once the secondary code is demodulated. This leads to longer coherent integration for a robust tracking. The presence of secondary codes on the pilot component mainly results in:

- Better autocorrelation properties of the pilot spreading code by making the overall period much longer
- Minimization of cross-correlation and improvement of narrowband interferences suppression through decreasing spectral lines [1]
- Providing of data message synchronization [2]

Additionally, GPS L1C secondary codes, which are especially very long, provide support for improved reading of clock and ephemeris [3] and decrease the number of time ambiguities after locking to the spreading codes [2].

The paper aims to discuss different secondary code structures, their autocorrelation properties and the probability of secondary code acquisition. Then the paper outline is as follows:

- The first section serves as a review of the studied GNSS signals and their main features. Several points differ from signals as L band frequency, spreading code length, code frequency, etc...
- The second section focuses on the secondary codes of the considered signals. Thus, it will be seen that each GNSS signal designers have chosen different secondary code lengths (between 20 and 1800 bits), which induces a different number of secondary codes (between 1 for short secondary codes and one per satellite for long secondary codes).
- The third section proposes a mathematical study on the probability of correct acquisition of the secondary code. This is based on the correlator output that contains the secondary code bits which is then correlated with the secondary code to highlight its first bit.
- The fourth section exploits Matlab simulation results to determine the threshold demodulation in terms of needed time and sensitivity. Then, the comparison between the four considered GNSS signals can be done based on the secondary code acquisition properties.
- Some conclusions are drawn in the last section by reminding the main results of the signals comparison and future works.

II. SIGNAL PROPERTIES

In the case of this study, four GNSS signals are considered: GPS L1C and L5 and Galileo E1 OS and E5a/b, whose frequency plans are presented in Fig. 1.

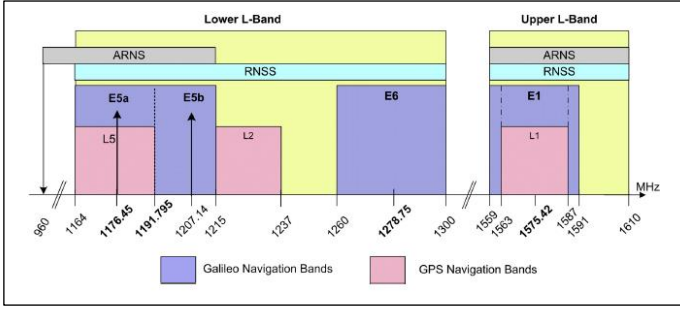


Fig. 1: GPS and Galileo frequency plans [4]

All the considered GNSS signals are composed of two components: one being the pilot component containing a secondary code. This section gives an overview of the main signal features. Table I and [5] summarize the main technical features which will be developed in this section.

TABLE I. SIGNAL FEATURES

Signal	Modulation	Central frequency	Spreading code length	Code frequency
GPS L1C	TMBOC (6,1,4/33)	1575.42 MHz	10230 chips 10 ms	1.023 MHz
GPS L5	BPSK(10)	1176.45 MHz	10230 chips 1 ms	10.23 MHz
Galileo E1 OS	CBOC (6,1,1/11)	1575.42 MHz	4092 chips 4 ms	1.023 MHz
Galileo E5	a	QPSK	10230 chips 1 ms	10.23 MHz
	b	QPSK	10230 chips 1 ms	10.23 MHz

A. GPS signals

1) GPS L1C signal

The GPS L1C signal is one of the new GPS signals and will be transmitted by the next generation of satellites, called GPS III, in 2014-2015. The GPS L1C design has been optimized to provide superior performance, while providing compatibility and interoperability with other signals in the L1 band (GPS L1 C/A but also Galileo E1 OS and QZSS) and improvements in receiver processing techniques.

GPS L1C, defined in [6] and detailed in [2] and [3], consists of two components. Both components are spread by a spreading code; the pilot channel is also modulated by a satellite (overlay) secondary code. There is one secondary code per satellite (210 secondary codes are defined but only 63 are used). This signal provides a number of advanced features, including a power difference in both components: 75% of power in the pilot component for enhanced signal tracking and 25% of power in the data component. At the end, the received signal is represented as follows:

$$r_{L1C}(t) = \left[\begin{array}{l} \frac{A}{2} \times d(t)c_{1,D}(t)p_{BOC(1)}(t) \\ + \frac{\sqrt{3}}{2} A \times c_2(t)c_{1,P}(t)p_{TMBOC}(t) \end{array} \right] \times \cos(2\pi(f_L + f_d)t + \phi_0) + n(t) \quad (1)$$

Where:

- d is the data sequence
- $c_{1,D}$ and $c_{1,P}$ are the spreading codes on the data and pilot component respectively
- c_2 is the studied secondary code
- $A = \sqrt{2C}$ is the total signal power
- f_L is the carrier frequency
- f_d is the Doppler frequency
- ϕ_0 is the initial phase of the signal
- n is the noise, assumed white Gaussian
- p_{BOC} and P_{TMBOC} are the subcarriers, which are defined by:

$$p_{BOC(x)}(t) = \text{sign}(\sin(2\pi \times x f_0 \times t))$$

$$p_{TMBOC}(t) = \begin{cases} p_{BOC(6)}(t) & \text{for 4 chips over 33} \\ p_{BOC(1)}(t) & \text{otherwise} \end{cases} \quad (2)$$

With t the time and $f_0 = 1.023$ MHz.

The GPS L1C implementation of TMBOC is produced by modulating in the pilot component 4 of each 33 spreading code chips (which number mod by 33 is in $\{1, 5, 7, 30\}$) with BOC(6,1) while retaining BOC(1,1) for all other spreading code chips in the pilot component (and also for all of the data spreading code chips). The spreading code is composed of 10230 chips and his period is 10 ms.

2) GPS L5 signal

The GPS L5 signal has been transmitted for the first time on board GPS IIF satellites. The GPS L5 carrier at 1176.45 MHz carries both components in quadrature. The GPS L5 signal presents the particularity to also have a tiered code on the data component, NH_{10} , it is a short code (10 bits) which lengthens the spreading code sequence. This 10-bit Neuman-Hofman will not be studied in this work as it is not on the pilot component.

The GPS L5 chipping rate of 10.23 MHz leads to a spreading code period of 1 ms (10 230 chips). The GPS L5 signal structure is given in (3) and for more details, refer to the ICD [7] and [8].

$$r_{L5}(t) = \frac{A}{\sqrt{2}} d(t)NH_{10}(t)c_{1,D}(t) \cos(2\pi(f_L + f_d)t + \phi_0) + \frac{A}{\sqrt{2}} c_2(t)c_{1,P}(t) \sin(2\pi(f_L + f_d)t + \phi_0) + n(t) \quad (3)$$

Where:

- NH_{10} is the Neuman-Hofman on the data component (10 bits)
- $c_2 = NH_{20}$ is the Neuman-Hofman on the pilot component (20 bits), the studied secondary code

B. Galileo signals

1) Galileo E1 OS signal

The Galileo E1 OS signal, the Galileo analog of GPS L1 C/A, is described in [4]. The data and pilot, in-phase, components are modulated by CBOC(6,1,1/11), which implies the use of two subcarriers (at f_0 and $6 \times f_0$) as defined in the Galileo E1 OS expression signal (4).

Galileo E1 OS differs from GPS signals (and Galileo E5 signals as it will be seen) by its spreading code period which is equal to 4 ms (for 4092 chips) instead of 1 or 10 ms.

$$r_{E1}(t) = \begin{bmatrix} \frac{A}{2} \times d(t)c_{1,D}(t)p_{CBOC,D}(t) \\ -\frac{A}{2} \times c_2(t)c_{1,P}(t)p_{CBOC,P}(t) \end{bmatrix} \times \cos(2\pi(f_L + f_d)t + \phi_0) + n(t) \quad (4)$$

Where $p_{BOC,D}$ and $p_{BOC,P}$ are the data and pilot subcarriers defined by:

$$\begin{aligned} p_{BOC,D}(t) &= \frac{\sqrt{10}}{\sqrt{11}}p_{BOC(1)}(t) + \frac{1}{\sqrt{11}}p_{BOC(6)}(t) \\ p_{BOC,P}(t) &= \frac{\sqrt{10}}{\sqrt{11}}p_{BOC(1)}(t) - \frac{1}{\sqrt{11}}p_{BOC(6)}(t) \end{aligned} \quad (5)$$

2) Galileo E5 a/b signal

The Galileo E5 signal is composed of four components and the signal power is divided evenly in 4. There are two data components (in-phase components): E5a-I and E5b-I which carry two different navigation message (F/NAV and I/NAV) and two associated pilot components (quadrature components): E5a-Q and E5b-Q. According to [4], the wideband Galileo E5 signal is generated with constant envelope Alternate Binary Offset Carrier (AltBOC) modulation. It is a modified version of BOC with code rate of 10.23 MHz and a subcarrier of 15.345 MHz. Because the two sidebands (E5a and E5b) can be processed independently, the Galileo E5 signal can also be considered as two separate Quadrature Phase Shift Keying (QPSK) signals with a carrier frequency of 1176.45 MHz and 1207.14 MHz (around the central frequency 1191.795 MHz). In the paper, to be equitable, Galileo E5a and Galileo E5b are considered as two signals then the power dedicated to each pilot component is similar to the power of Galileo E1 OS or GPS L5 pilot component (an half). Then, the Galileo E5 signal can be represented as follows:

$$\begin{aligned} r_{E5x-I}(t) &= \frac{A}{2}d_x(t)c_{x-I}(t)\cos(2\pi(f_L + f_d)t + \phi_{0,x-I}) \\ r_{E5x-Q}(t) &= \frac{A}{2}c_{2,x}(t)c_{x-Q}(t)\sin(2\pi(f_L + f_d)t + \phi_{0,x-Q}) \end{aligned} \quad (6)$$

Where:

- x stands for a or b
- $\phi_{0,x-I}$ and $\phi_{0,x-Q}$ are the initial phases

The spreading codes c_{x-I} and c_{x-Q} are sequences of 10230 chips which are spread in 1 ms at the code rate of 10.23 MHz.

III. SECONDARY CODE FEATURES

For the purpose of the presented study herein on the probability of secondary code acquisition, it is necessary, to first compare secondary code features (length and number of secondary codes) and secondary code autocorrelation properties (isolation).

For all of the GNSS signals, each bit of the secondary code is modulated to one period of the spreading code, the spreading code period, noted as T_c , (Table I) is equal to the secondary code bit duration (Table II).

TABLE II. SECONDARY CODE FEATURES

	Length	Bit duration	Number of secondary codes	Pilot Power allocations	A_β
GPS L1C-P	1800 bits 18 s	10 ms (100 b/s)	63	75% (- 1.25 dB)	$\frac{\sqrt{3C}}{\sqrt{2}}$
GPS L5-Q	20 bits 20 ms	1 ms (1 Mb/s)	1	50% (- 3 dB)	\sqrt{C}
Galileo E1-C	25 bits 100 ms	4 ms (250 b/s)	1	50% (- 3 dB)	\sqrt{C}
Galileo E5a-Q	100 bits 100 ms	1 ms (1 M b/s)	50	50% (-3 dB)	\sqrt{C}
Galileo E5b-Q	100 bits 100 ms	1 ms (1 M b/s)	50	50% (- 3 dB)	\sqrt{C}

The notation A_β is used to express the power of the pilot component.

As introduced, the paper focuses on the probability of secondary code acquisition. To do so, the secondary code autocorrelation function is defined:

$$R_{c_2}(\Delta) = \frac{1}{N} \sum_{i=1}^N c_2(i)c_2(i + \Delta) \quad (7)$$

Where N is the number of secondary code bits

Because the secondary code is a binary sequence of $+1$ and -1 , the autocorrelation function R_{c_2} is maximum for $\Delta = 0$ (the maximum value being 1). The other values taken by the autocorrelation function are more or less close to 0. The better autocorrelation function is in general for the one that has the lower values in absolute value; in other words, the higher isolation between the first maximum and the others.

A. GPS signals

1) GPS L1C signal

The pilot component of GPS L1C signal is modulated by secondary codes (one code per satellite) and called sometimes overlay code because it comes into play an overlaid on the pilot component. The length of the secondary codes is 1800 bits, which corresponds to the number of symbols on a data frame for L1C. One of the criteria used to create the family of the GPS L1C secondary codes was the good auto and cross-correlation properties.

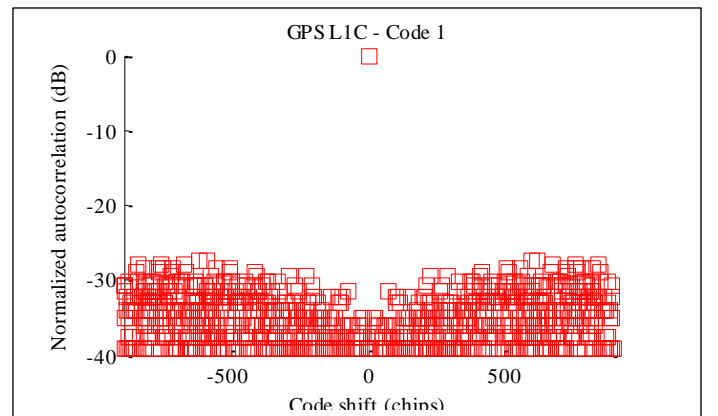


Fig. 2: GPS L1C (Code 1) normalized autocorrelation function

As it can be seen in Fig. 3 which gives the maximum normalized autocorrelation function for each satellite, the maximum autocorrelation is -24.78 dB (also given in [1] for even auto-correlation).

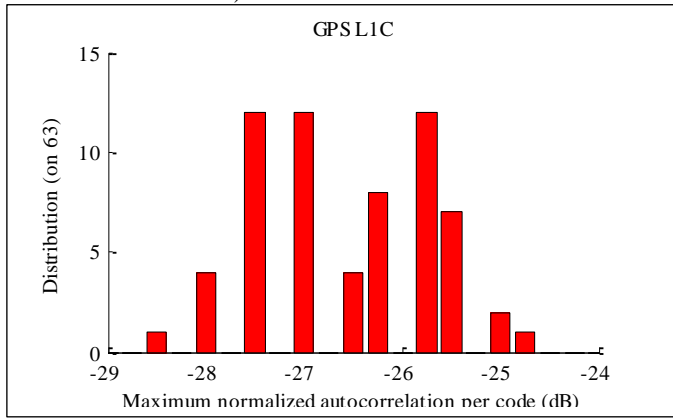


Fig. 3: Normalized autocorrelation maximum for all of the 63 GPS L1C secondary codes

2) GPS L5 signal

The GPS L1C secondary codes are the longest of the considered secondary codes and at the contrary, the GPS L5 secondary code is the shortest (20 bits). There is only one secondary code for GPS L5, NH_{20} .

TABLE III. GPS L5 SECONDARY CODE AUTOCORRELATION DISTRIBUTION

Autocorrelation function	Distribution		
	In dB	On 20	In %
$-\frac{4}{20} = -0.2$	-13.98 dB	3	15%
0	$-\infty$	14	70%
$\frac{4}{20} = 0.2$	-13.98 dB	2	10%
1	0 dB	1	5%

Due to its length, the GPS L5 secondary code autocorrelation properties cannot be as good as GPS L1C. Indeed, the maximum autocorrelation is only -13.98 dB as it is given in Fig. 4 and Table III which gives also the distribution.

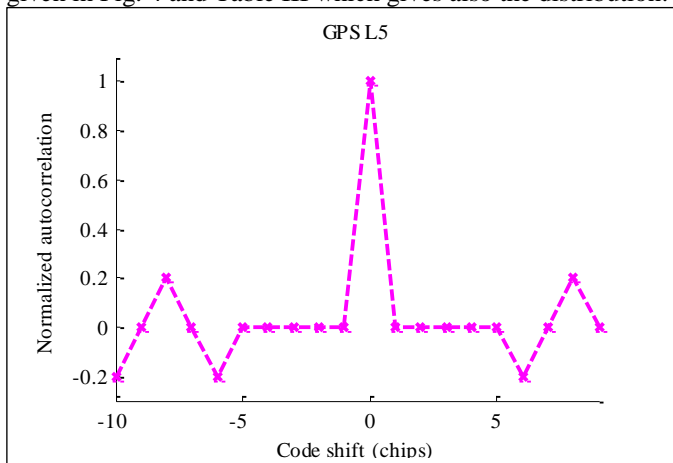


Fig. 4: GPS L5 secondary code autocorrelation function

B. Galileo signals

1) Galileo E1 OS signal

The Galileo E1 OS secondary code properties are close to GPS L5 secondary code ones. Indeed, there is only one Galileo E1 OS secondary code and its length is 25 bits. However, the maximum autocorrelation is higher: -18.42 dB.

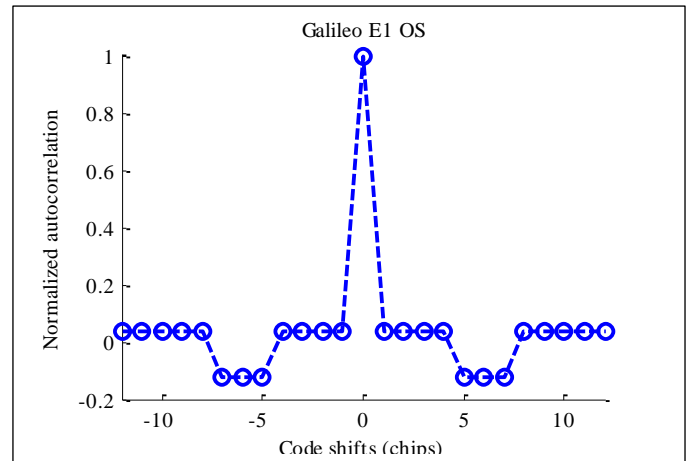


Fig. 5: Galileo E1 OS secondary code autocorrelation function

As GPS L5, Galileo E1 OS autocorrelation function is composed of a few values (3 for Galileo E1 OS and 4 for GPS L5).

TABLE IV. GALILEO E1 OS SECONDARY CODE AUTOCORRELATION DISTRIBUTION

Autocorrelation function	Distribution		
	In dB	On 25	In %
$\frac{1}{25} = 0.04$	-27.96 dB	18	72%
$-\frac{3}{25} = -0.12$	-18.42 dB	6	24%
1	0 dB	1	4%

2) Galileo E5 a/b signal

The short-duration primary code of Galileo E5 (1 ms) is balanced by a long-duration secondary code modulation [8]. The Galileo E5 secondary codes are predefined with sequences of lengths up to 100 bits. The autocorrelation properties of secondary codes are quite good and similar for Galileo E5a-Q and E5b-Q. The autocorrelation maximum is at -21.94 dB (the same for both Galileo E5 pilot components).

TABLE V. GALILEO E5A – CODE 1 AUTOCORRELATION DISTRIBUTION

Autocorrelation function	Distribution	
	In dB	On
0	$-\infty$	40
$\frac{4}{100} = 0.04$	-27.96 dB	49
$\frac{8}{100} = 0.08$	-21.94 dB	10
1	0 dB	1

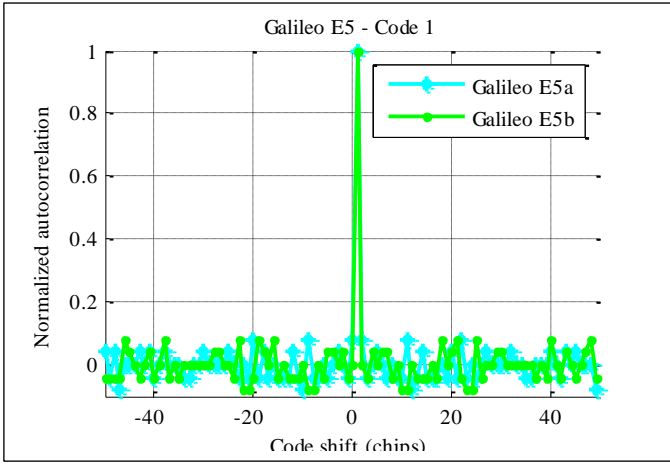


Fig. 6: Galileo E5 a/b-Q (first codes) autocorrelation function

Fig. 6 and 7 give the autocorrelation function for the first codes of Galileo E5a and E5b. For all of the Galileo E5 a and b secondary codes, the values taken by the secondary code autocorrelation function are the same and given in Table V. The difference between each code is the distribution (which slightly differs).

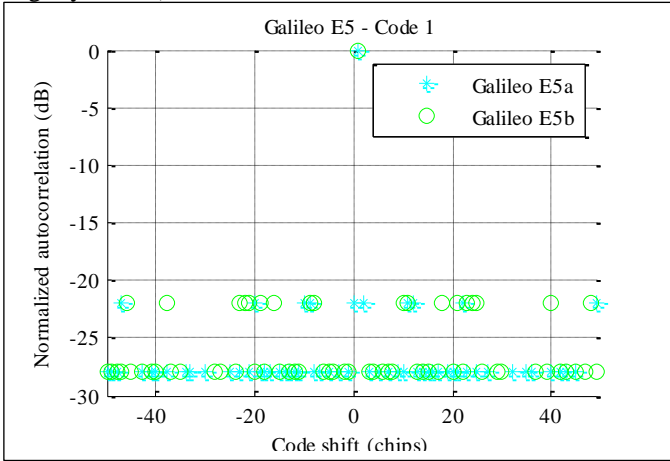


Fig. 7: Galileo E5a/b-Q (first code) autocorrelation function (in dB)

C. Secondary code comparison

Table VI summarizes the secondary code autocorrelation isolation for each secondary code.

TABLE VI. SECONDARY CODES AUTOCORRELATION ISOLATION

	Length (in bits)	Period (in ms)	Autocorrelation maximum	
			Real value in	(in dB)
GPS L1C-P	1800	1800	0.058	-24.78
GPS L5-Q	20	20	0.2	-13.98
Galileo E1-C	25	100	0.12	-18.42
Galileo E5a-Q	100	100	0.08	-21.94
Galileo E5b-Q	100	100	0.08	-21.94

As it can be seen, the minimum isolation is -13.98 dB. This value is obtained for GPS L5-Q, the shortest secondary code.

As it is understandable, the more the secondary code length is, the less the maximum autocorrelation is. Then, Galileo E1 OS seems to be a good compromise between secondary code length and autocorrelation isolation. Galileo E5 a/b has a better autocorrelation isolation for a longer secondary code (in bits) but similar secondary code period.

IV. PROBABILITY OF CORRECT ACQUISITION

Let us interest in the probability of correct acquisition of the secondary code.

A. Secondary code acquisition method

The successive secondary code bits are successively read and correlated with the actual secondary code (with a possible secondary code bit delay). The proposed method is detailed in three steps, each one is mathematically explained:

a) Acquiring the signal by giving an exact estimation of the code delay, Doppler frequency and phase of the incoming signal (using the autocorrelation function of the spreading code). The associated correlator output computation is given in Appendix A and its expressions is:

$$I(k, i) = \frac{A_\beta}{2} c_2(i) + n(k, i) \quad (8)$$

Where:

- $i \in \llbracket 1; N \rrbracket$ is the index of the considered secondary code bit
- $I(k, i)$ stands for the k th coherent summation on the i th secondary code bit: there are $N \times T_c$ ms between two successive integrations $I(1, i)$ and $I(2, i)$ on the i th bit
- $n(k, i)$ can be modeled as a centered Gaussian noise with a variance equal to $\frac{N_0}{4T_c}$ [9]

Let us remark that here the phase error is assumed to be null, in the section V.C, some results are presented assuming a more realistic case, that means with a residual phase tracking error; the mathematical development when considering a not null phase error is given Appendix B.

b) The technique can be enhanced by coherent accumulation over the duration of several secondary code periods. Mathematically, the summation over the i th secondary code bit is:

$$\begin{aligned} I_K(i) &= \frac{1}{K} \sum_{k=1}^K I(k, i) \\ &= \frac{A_\beta}{2} \times \frac{1}{K} \sum_{k=1}^K c_2(i) + \frac{1}{K} \sum_{k=1}^K n(k, i) \\ &= \frac{A_\beta}{2} \times c_2(i) + n_K(i) \end{aligned} \quad (9)$$

This leads to a reduction in noise impact because the resulting noise $n_K(i)$ is a Gaussian distribution with null mean and a variance equal to $\frac{N_0}{4KT_c}$. It can be seen as the coherent integration on $K \times T_c$ ms.

Then, $\hat{c}_2(i)$, the normalized $I_K(i)$ correlator output by $A_\beta/2$ can be seen as an estimator of the i th secondary code bit $c_2(i)$.

(9) becomes:

$$\widehat{c}_2(i) = \frac{I_K(i)}{A_B/2} = c_2(i) + n'_K(i) \quad (10)$$

The noise n'_K is a Gaussian distribution with null mean and the variance is given by (11) and represented in Fig. 8.

$$\sigma^2 = \text{var}(n'_K) = \frac{1}{(A_B/2)^2} \times \frac{N_0}{4KT_c} \quad (11)$$

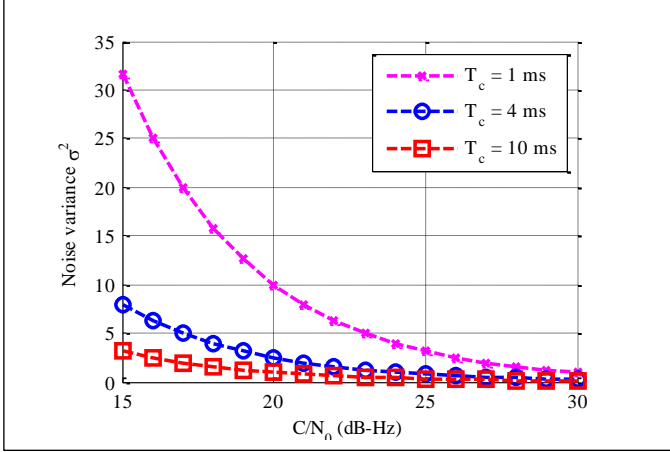


Fig. 8: Noise variance versus the C/N₀

c) The last step is the correlation with secondary code to perform the determination of the bit delay, noted as Δ (it can be seen as $i' - \Delta$)

$$\begin{aligned} \widehat{R}_{c_2}(\varepsilon_\Delta) &= \frac{1}{N} \sum_{i=1}^N \widehat{c}_2(i) \times c_2(i - \widehat{\Delta}) \\ &= \frac{1}{N} \sum_{i=1}^N c_2(i) c_2(i - \widehat{\Delta}) + \frac{1}{N} \sum_{i=1}^N n'_K(i) c_2(i - \widehat{\Delta}) \\ &= R_{c_2}(\varepsilon_\Delta) + n(\widehat{\Delta}) \end{aligned} \quad (12)$$

At the end, the noise $n(\widehat{\Delta})$ is a Gaussian distribution with null mean. The variance of $n(\widehat{\Delta})$ is σ^2/N . Noises for each point of $\widehat{R}_{c_2}(\varepsilon_\Delta)$ are identically distributed but there are not independent. Indeed, due to the correlation with the same noise sequence n'_K , the correlation term, given by the covariance (12), corresponds to the autocorrelation function. Then, for Δ_1 different from Δ_2 :

$$\text{cov}(n(\Delta_1), n(\Delta_2)) = R_{c_2}(|\Delta_1 - \Delta_2|) \quad (13)$$

B. Probability of correct secondary code acquisition

The probability of correct secondary code acquisition consists in evaluating the probability to estimate in a right way the parameter Δ that means to find the first bit of the secondary code. To determine it, the maximum secondary code autocorrelation function is studied. Then the probability of correct secondary code acquisition is equivalent to the probability that the maximum value of $\widehat{R}_{c_2}(\varepsilon_\Delta)$ is for ε_Δ such as $R_{c_2}(\varepsilon_\Delta) = 1$.

It is then appropriate to mathematically develop the probability of secondary code acquisition even if the obtained expression is not as simple as it is wanted. Let us note X_i , for

$i = 1, \dots, N$ the output of $\widehat{R}_{c_2}(\varepsilon_\Delta)$ for $\varepsilon_\Delta = |i - \widehat{\Delta}|$. Their distributions are $\mathcal{N}\left(\mu_i, \frac{\sigma^2}{N}\right)$ with $\mu_i = R_{c_2}(|i - \widehat{\Delta}|)$, the mean. The cumulative distribution function of X_i is this of a normal distribution:

$$F_{X_i}(x) = P(X_i \leq x) = \frac{1}{2} \left(1 + \text{erf}\left(\frac{x - \mu_i}{\sqrt{2\sigma^2}}\right) \right) \quad (14)$$

Where the error function $\text{erf}(\cdot)$ is defined by:

$$\text{erf}(z) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^z e^{-t^2/2} dt \quad (15)$$

Then, the density of probability $f_{X_1} = dF_{X_1}$ is given by:

$$f_{X_i}(x) = \frac{1}{\sqrt{2\pi\sigma^2}} e^{-\frac{(x-\mu_i)^2}{2\sigma^2}} \quad (16)$$

To develop the mathematical model, let us assume that there is no bit delay, then X_1 is the only random variable such as $\mu_1 = 1$. Let us introduce Y the random variable which is the maximum of the others X_i : $Y = \max_{i=2, \dots, N} X_i$.

Now, the probability of secondary code acquisition, denoted as P_a is:

$$P_a = P(X_1 \geq Y) = P\left(X_1 \geq \max_{i=2, \dots, N} X_i\right) \quad (17)$$

To evaluate P_a , let us first determine the distribution of the random variable Y , by evaluating cumulative distribution function, F_Y . To do so, the independence between the random variables X_i is supposed, it can be done because the autocorrelation function is close to 0 (section III.C).

$$\begin{aligned} F_Y(y) &= P(Y \leq y) = P\left(\max_{i=2, \dots, N} (X_i) \leq y\right) \\ &= P(\forall i = 2, \dots, N, X_i \leq y) \\ &= \prod_{i=2}^N P(X_i \leq y) = \prod_{i=2}^N F_{X_i}(y) \\ &= \frac{1}{2^{N-1}} \prod_{i=2}^N \left(1 + \text{erf}\left(\frac{y - \mu_i}{\sqrt{2\sigma^2}}\right) \right) \end{aligned} \quad (18)$$

Then, the probability of secondary code acquisition can be computed knowing the distribution of $Y = \max_{i=2, \dots, N} X_i$ and X_1 .

$$\begin{aligned} P_a &= P(X_1 > Y) \\ &= \int_{\mathbb{R}} P(X_1 - Y > 0 | X_1 = x) dF_{X_1}(x) \\ &= \int_{\mathbb{R}} P(x - Y > 0 | X_1 = x) dF_{X_1}(x) \\ &= \int_{\mathbb{R}} P(x > Y) dF_{X_1}(x) = \int_{\mathbb{R}} P(Y < x) dF_{X_1}(x) \\ &= \int_{\mathbb{R}} F_Y(x) f_{X_1}(x) dx \\ &= \frac{1}{2^{N-1}} \frac{1}{\sqrt{2\pi\sigma^2}} \int_{\mathbb{R}} \prod_{i=2}^N F_{X_i}(y) e^{-\frac{(x-\mu_i)^2}{2\sigma^2}} dx \end{aligned} \quad (19)$$

It is extremely difficult to check and exploit this expression (Mathematica can provide an approximation by means of numerical analysis to approach the integral).

Anyway, it can be understood that the probability of correct secondary acquisition P_a depends on the considered signal through:

- The integration time, which corresponds to the spreading code period T_c (1, 4 or 10 ms)
- The secondary code length N (20, 25, 100 or 1800 bits)
- The carrier to noise density C/N_0 through $\frac{A_B}{\sqrt{N_0}}$
- The values taken by the secondary code autocorrelation function $R_{c_2}(|i - \hat{\Delta}|)$

The other parameter is the number of coherent accumulations $K \geq 1$. The objective is to determine K for which the probability of correct secondary code acquisition is satisfying (higher to 0.99). Then, the required time to correct acquire the secondary code can be computed. It is the number of coherent accumulations K multiplied by the secondary code period (in ms).

V. SIMULATION RESULTS

A. Simulation scheme

The simulation scheme consists in evaluating the probability of secondary code acquisition depending on the total received signal power and on the required time. To do so, the secondary code estimator as defined in (10) is simulated as the secondary code plus a random noise with null mean and a variance of σ^2 . Then, the correlation function with a local secondary code is computed using:

$$\widehat{R}_{c_2} = \frac{1}{N} \mathcal{F}^{-1}(\mathcal{F}(c_2) \times \overline{\mathcal{F}(\widehat{c}_2)}) \quad (20)$$

Where \mathcal{F} is the discrete Fourier Transform operator

Based on the output of the correlation operation, the successful secondary code acquisition is declared when the highest point of the correlation function corresponds to the correct synchronization. Matlab simulations are run a large number of times (10 000) to determine the probability of correct secondary code acquisition (the ratio of correct detection of the maximum over the number of runs).

B. Simulation results considering perfect phase tracking

In a first time, the simulations are run assuming that the carrier phase tracking is perfect. Two results are investigated:

- The first one is the probability of secondary code acquisition on one secondary code period.
- The second result consists in studying the required acquisition time to reach a probability of secondary code acquisition greater than 99% for a given C/N_0 .

The simulation results are presented by means of tables and figures: the parameter C/N_0 , for figures, represents the total received signal power to compare the signals performance and for tables the pilot component power to compare secondary codes not influenced by the difference on the power on the pilot component.

1) K set to 1

The first result is the probability of correct secondary acquisition knowing that K is set to 1 (the secondary code is only read once) and for three values of C/N_0 .

As it can be anticipated, the GPS L1C signal (in red) is the best one in terms of probability of secondary code acquisition for a given C/N_0 . This is mainly due to the very long secondary code period (18 s) compared to the others (around 100 ms). It also represents a case that might be optimistic as GPS L1C receiver might use another acquisition technique (such as partial correlation) to speed up the acquisition.

GPS L5 and Galileo E1 OS have secondary codes properties and pilot component power shares that are close but their probabilities of secondary code acquisition present notable differences. Indeed, for a given probability of acquisition, there can be a difference of 5 dB and for the same C/N_0 , there can be a difference of 0.2 on the probability of acquisition, Galileo E1 OS (in blue) being the best. This can be explained by the variance of the noise which is higher for smallest values of T_c (as pointed out in Fig. 8).

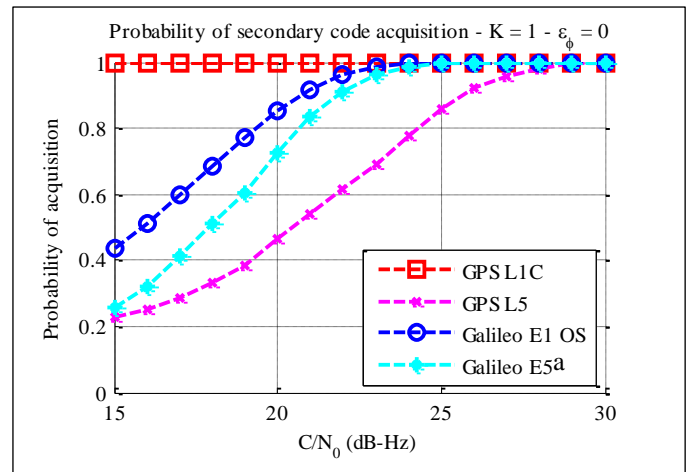


Fig. 9: Probability of secondary code acquisition for 1 coherent accumulation

The probabilities of secondary code acquisition for each Galileo E5 secondary codes are very similar (difference lower than 0.025), then Galileo E5a-Q is not differentiated from Galileo E5b-Q and is represented in cyan. It is between the probabilities of secondary codes acquisition for GPS L5 and Galileo E1 OS. Then, for the same secondary code period (100 ms), Galileo E1 OS is better than Galileo E5a, mainly due to the variance depending on the spreading code period.

Table VII. PROBABILITY OF ACQUISITION (POWER OF THE PILOT COMPONENT)

	Probability of acquisition		
	15 dB-Hz	20 dB-Hz	25 dB-Hz
GPS L1C-P	1	1	1
GPS L5-Q	0.2614	0.5501	0.9298
Galileo E1-C	0.6948	0.9835	1
Galileo E5a-Q	0.4947	0.9574	1
Galileo E5b-Q	0.4957	0.9589	0.9999

To take into account the difference of power on the pilot component, Table VII is given. The probability of secondary code acquisition is given depending on the power on the pilot component. As discussed in previous figure, GPS L1C is the better one followed by Galileo E1 OS. Galileo E5 is between GPS L5 and Galileo E1 OS in terms of probability of secondary code acquisition.

2) Probability of desired secondary code acquisition set to 0.99

The second result consists in estimating the required time to correctly (with a probability of 99%) acquire the secondary code. Fig. 10 presents results for GPS L5, Galileo E1 and E5; GPS L1C is not considered since it has been seen in the previous section that the probability of secondary code acquisition is equal to 1 whichever the considered C/N_0 above 15 dB-Hz.

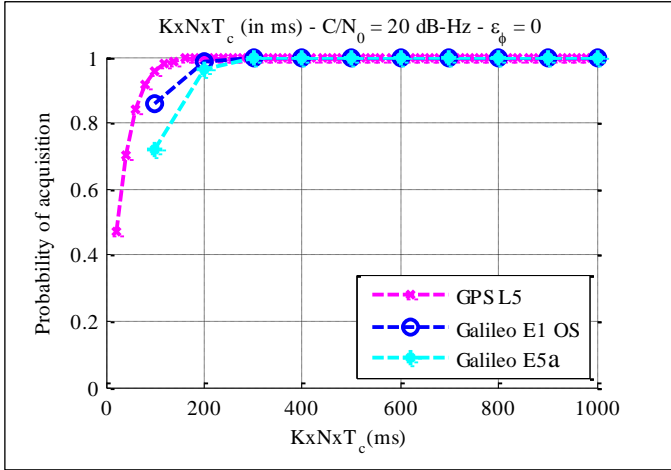


Fig. 10: Required time to reach a high probability of secondary code acquisition

The Galileo E5a needs more time than GPS L5 and Galileo E1OS which are very close because for low C/N_0 . The Galileo E5a probability of secondary code acquisition is close to the one of GPS L5 but the secondary code period is longer than GPS L5 secondary code period. The GPS L5 secondary code period is shorter (20 ms) than the Galileo E1 OS or E5a and b secondary code period (100 ms); this explains why the GPS L5 seems to be a curve whereas Galileo E1 and E5a seem to be a line and then results. Table VIII, which provides the required time to reach a given probability of secondary code acquisition for a given received pilot component power of C/N_0 completes the results presented previously.

TABLE VIII. REQUIRED TIME TO A PROBABILITY OF ACQUISITION OF 99% (20 dB-HZ ON THE PILOT COMPONENT)

	K	$K \times N \times T_c$ (in ms)
GPS L1C-P	1	18000
GPS L5-Q	6	120
Galileo E1-C	2	200
Galileo E5a-Q/ E5b-Q	2	200

For the same secondary code period (100 ms) for Galileo E1 and E5, the required time to reach the probability of secondary code acquisition of 99% is the same, namely two secondary code periods. GPS L5 needs more coherent accumulations but because GPS L5 secondary code is shorter (20 ms), the total required time is lower.

C. Simulation results considering realistic phase tracking

After studying the better case –with a null phase error–, let us interest in the more realistic case. The phase error represents the error between the incoming signal carrier phase and the local one. ε_ϕ follows a Gaussian distribution [10] with a null average and a variance defined by [8]:

$$\sigma_{\varepsilon_\phi}^2 \approx \frac{B_L}{C/N_0} \left(1 + \frac{1}{2T_c C/N_0} \right) \quad (\text{rad}^2) \quad (21)$$

The mathematical model is developed in Appendix B. Then, for realistic simulation results, the term in $\left(\frac{\sum_{k=1}^K \cos(\varepsilon_\phi)}{K} \right)$ will have a not negligible impact on the secondary code acquisition performance.

For secondary code demodulation, as it is done for data demodulation, the first correlator output computation and the second one for the same secondary code bit is delayed by the secondary code period. Then, phase errors can be supposed to be uncorrelated because the secondary code period is largely greater than the loop convergence time. Then, for simulations, the phase error is supposed to be a centered Gaussian distribution with the variance given by (21). The secondary code is correlated with a secondary code sequence affected by $\left(\frac{\sum_{k=1}^K \cos(\varepsilon_\phi)}{K} \right)$ plus noise. For one coherent integration, each secondary code bit is multiplied by $\cos(\varepsilon_\phi)$, for two coherent integrations, it is multiplied by the average of two cosine terms, etc... Let us remark that if the ε_ϕ follows a Gaussian distribution, $\left(\frac{\sum_{k=1}^K \cos(\varepsilon_\phi)}{K} \right)$ seems to be also a Gaussian distribution even if $\cos(\varepsilon_\phi)$ is not distributed as a Gaussian.

When the phase error is greater than 1 rad, the tracking loops lose lock. For a C/N_0 of 15 dB-Hz, only 80% of the randomly generated phase errors are lower than 1 radian. As a consequence, a C/N_0 above 20 dB-Hz is considered because lesser than 2% of the values are greater than 1 radian. Fig. 11 provides the probability of secondary code acquisition when considering phase tracking error.

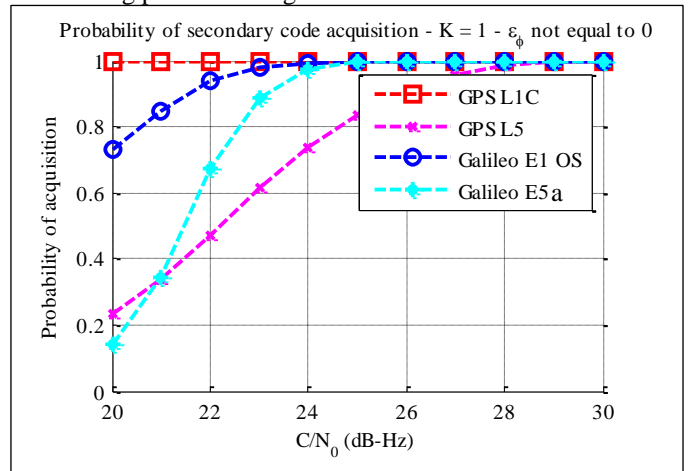


Fig. 11: Probability of secondary code acquisition for 1 coherent accumulation and a not null phase error

The variance of the phase error is inversely proportional to the sensitivity and to the spreading code period T_c . Then, as it is the case for the noise variance in Fig. 8., the variance is maximal for T_c equal to 1 ms. At 20 dB-Hz, in the worst case, for GPS L5 and Galileo E5a, the variance is 0.6 rad compared with 0.225 for Galileo E1 OS and 0.15 for GPS L1C. This results in higher degradations in the probability of secondary code acquisition (Fig. 11) and for a given C/N_0 more time to reach the same probability of secondary code acquisition (Fig. 12) for the L5 band GNSS signals.

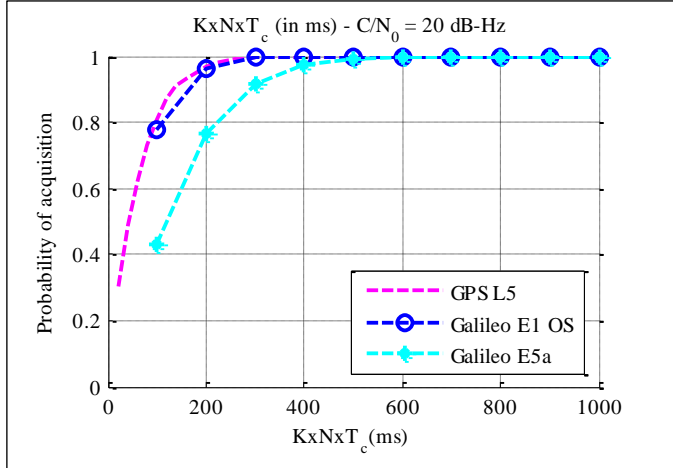


Fig. 12: Required time to reach a high probability of secondary code acquisition considering a not null phase error

The case GPS L1C is not discussed because one coherent integration is 18 seconds which is largely outside of reasonable acquisition time interval. When considering not null phase error and for all of the other signals, GPS L5 secondary code needs 260 ms to be acquired 99% of time. Due to a longer secondary code period, Galileo E1 OS needs 300 ms. Galileo E5a needs more time (500 ms) because it suffers from relatively long secondary code period (as Galileo E1 OS) but a higher variance value compared to Galileo E1 OS.

For the same given C/N_0 of 20 dB-Hz, the probability of Galileo E5 secondary code acquisition becomes 0.14 (Fig. 11) when considering phase error instead of 0.4 (Fig. 9) when the assumption of no phase error is done. This explains the considerable expansion of the required time to reach the same probability.

VI. CONCLUSION

In this paper, a study on secondary codes was done. Four secondary code classes (GPS L1C, GPS L5, Galileo E1 OS and Galileo E5a/b) are compared in terms of autocorrelation.

In a first part, the features of each one are reminded. The length of secondary codes can be very different between 20 and 1800 bits, which implies different secondary code autocorrelation isolation properties. Indeed, for the GPS L1C, which is the longest secondary code (1800 bits), the isolation is 24.78 dB but for the GPS L5, which is the shortest secondary code (20 bits), the isolation is only 13.98 dB (more than 10 dB of difference). The Galileo E1 OS seems to be a good compromise between secondary code length and

isolation; with 25 bits, the isolation is 18.42 dB. The GPS L5 secondary period (20 ms) is 5 times lower than the Galileo E1 OS and E5 (100 ms) and 90 times than the GPS L1C secondary code period.

Then, the paper focuses on the probability of secondary code acquisition. Simulation provides results in terms of probability of secondary code acquisition versus the secondary code acquisition time and sensitivity. Due to its length, the GPS L1C secondary code provides the better probability of secondary code acquisition for a given sensitivity (even low) but 18 seconds are required. The Galileo E1 OS is still one of the most interesting compromise between probability of secondary acquisition and required time, due to its spreading code period (secondary code bit) which is longer than the one of GPS L5 and Galileo E5. Indeed, the Galileo E5 secondary code acquisition performance depends on the considered sensitivity (total signal power or only one pilot component power). Even if the better case is considered (pilot component power), the Galileo E5 secondary code acquisition performance is not as better as Galileo E1 OS which has the same secondary code period. The GPS L5 secondary code acquisition performance is quite good due to its short secondary code period (only 20 ms).

As seen, the assumption of perfect phase tracking is an ideal case because when considering phase tracking error, the performance of secondary code acquisition is degraded: some more coherent integrations are needed to reach the probability of 99% of secondary code acquisition: 3 for Galileo E5a, 1 for Galileo E1 OS and around 5 for GPS L5.

In the context of this study, it is difficult to compare the GPS L1C due to its very long secondary code period. Galileo E1 OS is better than Galileo E5 and maybe the one which proposes the best compromise between secondary code period (which implies secondary code acquisition time) and probability of secondary code acquisition.

For the special case of GPS L1C, it may be interesting to study secondary code acquisition by means of partial correlations. In a first time, the number of kept secondary code bits (completed by zero bits to reach the length of 1800 bits) should be determined to provide reasonable isolation: 125 bits are sufficient to reach an approximate isolation of -14 dB (GPS L5 secondary code autocorrelation isolation) but it corresponds to 1.25 second. To reach the Galileo E5a secondary code autocorrelation isolation, a zero-padding of an half of the length of the GPS L1C secondary code is sufficient but at least 8 seconds are needed. Then, the reduction in number of bits is interesting but still leads to long partial correlations.

This work focuses on GPS and Galileo signals, two signals are not studied: GPS L2C and Galileo E6, for commercial service, which contain a pilot component but they do not carry a secondary code. The work can be extended to the other GNSS constellations, namely Glonass, QZSS, Beidou...

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A. Classical acquisition correlator output

The GNSS incoming signal can be modeled as:

$$r(t - \tau) = \begin{bmatrix} A_\alpha d(t - \tau) c_{1,D}(t - \tau) p_D(t - \tau) \\ + A_\beta c_2(t - \tau) c_{1,P}(t - \tau) p_P(t - \tau) \end{bmatrix} \times \cos(2\pi(f_{IF} + f_d)t + \phi_0) + n(t)$$

Where:

- τ and f_d are the incoming code delay and Doppler frequency which are locally estimated by \hat{f}_d and $\hat{\tau}$
- A_α and A_β are the power on the data and pilot component

Let us denote T_c the spreading code period, N the length of the secondary code, k the coherent summation number and $i \in \llbracket 1; N \rrbracket$ the index for the considered secondary code bit. Then, the k th inphase correlator output of the i th secondary code bit results in the integration of the incoming signal multiplied by a local replica of the pilot sequence (pilot spreading code and pilot subcarrier).

$$\begin{aligned} & I(k, i) \\ = & \frac{1}{T_c} \int_{(Nk+i)T_c}^{(Nk+(i+1))T_c} r(t - \tau) \times \\ & c_{1,P}(t - \hat{\tau}) p_P(t - \hat{\tau}) \cos(2\pi(f_{IF} + \hat{f}_d)t) dt \\ \approx & \begin{bmatrix} \frac{A_\beta}{2} d(k, i) R_{cross}(\varepsilon_\tau(k, i)) \\ + \frac{A_\beta}{2} c_2(i) R_{c_{1,P}}(\varepsilon_\tau(k, i)) \end{bmatrix} \\ & \times \cos\left(2\pi\varepsilon_f(k, i) \left(i + \frac{1}{2}\right) + \varepsilon_\phi(k, i)\right) \text{sinc}\left(\pi T_c \varepsilon_f(k, i)\right) \\ & - \int_{(Nk+i)T_c}^{(Nk+(i+1))T_c} n(t) c_{1,P}(t - \hat{\tau}) p_P(t - \hat{\tau}) \cos(2\pi\hat{f}t + \hat{\phi}) dt \\ \approx & \frac{A_\beta}{2} c_2(i) \cos(\varepsilon_\phi(k, i)) + n(k, i) \end{aligned}$$

Where :

- $\varepsilon_f(k, i)$ and $\varepsilon_\tau(k, i)$ are assumed to be null (right Doppler frequency and code estimation) because the acquisition stage is supposed to be done
- $R_{cross}(\cdot)$ is the cross-correlation (between the data and pilot spreading codes) and is supposed to be null
- $\varepsilon_\phi(k, i)$ is phase error

The received noise is assumed to be white and Gaussian with a noise level of N_0 . Then at the correlator output, the noise $n(k, i)$ is assumed to be Gaussian with null mean and its variance is equal to $\frac{N_0}{4T_c}$ (refer to [9]).

The same correlation process can be done for pilot component in quadrature: the received signal is multiplied by $c_{1,P}(t - \hat{\tau}) p_P(t - \hat{\tau}) \sin(2\pi(f_{IF} + \hat{f}_d)t)$ and the same correlator output $\frac{A_\beta}{2} c_2(i) \cos(\varepsilon_\phi(k, i)) + n(k, i)$ is obtained.

B. Secondary code acquisition considering phase error tracking

In this appendix, the secondary code acquisition steps are developed again but considering phase error:

a) Acquiring the signal by giving an exact estimation of the code delay and Doppler frequency of the incoming signal (using the autocorrelation function of the spreading code). The associated correlator output computation is given in and its expressions is:

$$I(k, i) = \frac{A_\beta}{2} c_2(i) \cos(\varepsilon_\phi) + n(k, i)$$

Where:

- ε_ϕ is the phase tracking error. In the context of this paper, neglecting the effect of the local oscillator phase noise, it is assumed to have a variance [8] equal to

$$\sigma_{\varepsilon_\phi}^2 \approx \frac{B_L}{C/N_0} \left(1 + \frac{1}{2T_c C/N_0}\right) \text{ (rad}^2\text{)}$$

Where

- B_L , the carrier loop noise bandwidth chosen to be equal to $B_L = 10$ Hz.

b) The technique can be enhanced by coherent accumulation over the duration of several secondary code periods. Mathematically, the summation over the i th secondary code bit is:

$$\begin{aligned} I_K(i) &= \frac{1}{K} \sum_{k=1}^K I(k, i) \\ &= \frac{A_\beta}{2} \times \frac{1}{K} \sum_{k=1}^K c_2(i) \cos(\varepsilon_\phi) + \frac{1}{K} \sum_{k=1}^K n(k, i) \\ &= \frac{A_\beta}{2} \left(\frac{\sum_{k=1}^K \cos(\varepsilon_\phi)}{K} \right) \times c_2(i) + n_K(i) \end{aligned}$$

This leads to a reduction in noise impact because the resulting noise $n_K(i)$ is a Gaussian distribution with null mean and a variance equal to $\frac{N_0}{4KT_c}$. It can be seen as the coherent integration on $K \times T_c$ ms.

Then, $\hat{c}_2(i)$, the normalized $I_K(i)$ correlator output by $\frac{A_\beta}{2}$ can be seen as an estimator of the i th secondary code bit $c_2(i)$. becomes:

$$\hat{c}_2(i) = \frac{I_K(i)}{\frac{A_\beta}{2}} = c_2(i) \left(\frac{\sum_{k=1}^K \cos(\varepsilon_\phi)}{K} \right) + n'_K(i)$$

c) The last step is the correlation with secondary code to perform the determination of the bit delay, noted as Δ (i can be seen as $i' - \Delta$)

$$\begin{aligned} \widetilde{R}_{c_2}(\varepsilon_\Delta) &= \frac{1}{N} \sum_{i=1}^N \hat{c}_2(i) \times c_2(i - \widehat{\Delta}) \\ &= \frac{1}{N} \sum_{i=1}^N c_2(i) \left(\frac{\sum_{k=1}^K \cos(\varepsilon_\phi)}{K} \right) c_2(i - \widehat{\Delta}) + \frac{1}{N} \sum_{i=1}^N n_K(i) c_2(i - \widehat{\Delta}) \\ &= \widetilde{R}_{c_2}(\varepsilon_\Delta) + n(\widehat{\Delta}) \end{aligned}$$

Where \widetilde{R}_{c_2} is an approximate of the autocorrelation function

At the end, the noise $n(\widehat{\Delta})$ is a Gaussian distribution with null mean. The variance of $n(\widehat{\Delta})$ is σ^2/N .